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May 31, 2018

Village of West Alexandria 16 North Main Street West Alexandria, Ohio 45381

Attention: Mayor Carol Lunsford – Village of West Alexandria

Reference: Geotechnical Exploration Report West Alexandria WWTP West Alexandria, Preble County, Ohio CTL Project No. 18050006CIN

Dear Mayor Lunsford:

CTL Engineering, Inc. has completed the geotechnical exploration report for the above referenced project. We are providing a digital version (PDF file) of this engineering report via email.

Thank you for the opportunity to provide these services for this project. If you have any questions, please contact our office.

Respectfully Submitted,

CTL ENGINEERING, INC.

Doug R. Batt, P.E. Project Manager

GEOTECHNICAL EXPLORATION REPORT

WEST ALEXANDRIA WASTEWATER TREATMENT PLANT WEST ALEXANDRIA, PREBLE COUNTY, OHIO

CTL PROJECT NO. 18050006CIN

PREPARED FOR:

VILLAGE OF WEST ALEXANDRIA 16 NORTH MAIN STREET WEST ALEXANDRIA, OHIO 45381

PREPARED BY:

CTL ENGINEERING, INC. 2105 SCHAPPELLE LANE CINCINNATI, OHIO 45240

MAY 31, 2018



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I. <u>PROJECT LOCATION AND DESCRIPTION</u>

The overall project involves the construction of a new wastewater treatment plant consisting of new structures which are located south-southwest of the existing West Alexandria Wastewater Treatment Plant which is located at the south end of Desota Drive in West Alexandria, Preble County, Ohio.

The treatment plant improvements are listed in Table 1 below along with the preliminary bottom of structure/finish floor elevation, estimated plan dimensions and the corresponding test borings drilled in the vicinity of the structures. Piping and related utility lines between these structures as well as a parking area and a roadway around the boundary of the site are also planned.

			Structure	Structure	
	Boring	Approximate Depth of	Plan Dimensions	Bearing Flevation	Structure/ Foundation
Structure	ID No.	Structure, ft	ft	ft	Description
Lab/Admin Building	9, 14, 15	4	40 x 30	881	Single Story Masonry Structure/Stri p Footings
Oxidation Ditch	2, 3, 7, 8, 12, 13	10	100 x 34	875	Concrete Structure/Mat Foundation
Screen Building	8	8	27 x 6	877	Concrete Structure/Mat Foundation
Aerobic Digester Tanks	3, 4, 9	16	60 x 16	869	Concrete Structure/Mat Foundation
Clarifier Tanks	1, 5, 6, 11	19	40 (diameter)	861.5 – 864.5	Concrete Structure/ Circular Mat Foundation
UV Disinfection	10	8	40 x 5	871.5	Concrete Structure/Mat Foundation

Table 1. Test Boring and Proposed Structure Information

CTL Engineering, Inc. (CTL) understands that the general purpose of the geotechnical exploration is to determine the subsurface conditions of the site in conjunction with evaluating its suitability for construction of the proposed plant improvements.



II. <u>SUBSURFACE EXPLORATION</u>

Eighteen (18) test borings, designated as B-01-18 through B-18-18, were drilled at the locations shown on the enclosed boring location plan that is attached to this report in Appendix C. The test borings were originally planned for a facility layout that has since been revised. The boring location plan in Appendix C presents the locations of the drilled test borings relative to the proposed structures as identified in Table 1 above. These test borings were drilled to planned depths ranging from 10 feet to 35 feet below the existing ground surface (bgs). The number of test borings and their planned depths were determined by Jones & Henry Engineers (J&H) with input from CTL. Kramer & Associates (project surveyor) located the test borings in the field and determine the coordinates along with the corresponding ground surface elevations. The test boring coordinates and ground surface elevations were provided to CTL by J&H.

The test borings were drilled on March 22 through 28, 2018 by CTL, utilizing hollow stem augers powered by a track-mounted rotary drill rig. Standard Penetration Tests (SPTs) were conducted in the test borings using a 140-pound automatic hammer falling 30 inches to drive a 2-inch O.D. split barrel sampler for 18 inches. The SPTs and split-barrel (spoon) sampling were performed at 2.5 feet and 5 feet intervals to the boring termination depths. In addition, an undisturbed (Shelby) tube sample was obtained at a selected location and depth.

Soil samples obtained from drilling operations were preserved in glass jars, visually classified in the field, and delivered to CTL's materials laboratory for testing and analysis. Representative samples were subjected to laboratory testing including natural moisture content, Atterberg Limits, and particle size analysis. The undisturbed sample's unit weight along with an unconfined compressive strength test was performed on the recovered sample.

Drilling, sampling, field and laboratory testing have been performed according to standard geotechnical engineering practices and current ASTM procedures. Results from the field testing are shown on the enclosed test boring records in Appendix A, and laboratory test results are presented in Appendix B.

III. <u>FINDINGS</u>

A. <u>Geology</u>

According to the <u>Web Soil Survey: Preble County, Ohio (OH135)</u>, *United States Department of Agriculture, Natural Resources Conservation Service*, surficial soils mapped at the subject site are described in the table below.



Soil Series	Series Symbol	Drainage Characteristics	Corrosivity Potential Concrete / Steel
Fox silt loam, till substratum 0 to 2 percent slopes	FmA	Well drained with a low runoff class	Low / High
Kendallville-Eldean silt loams, 6 to 12 percent slopes, eroded	KeC2	Well drained with a medium runoff class	Low / Low
Rainsville silt loam, 2 to 6 percent slopes	RaB	Well drained with a low runoff class	Moderate / High
Rodman gravelly loam, 18 to 25 percent slopes, eroded	RnE2	Excessively drained with a medium runoff class	Low / Low

Mapping of the bedrock topography (<u>Bedrock Topography of the West</u> <u>Alexandria, Ohio, Quadrangle, ODNR Geological Survey, Digital Map Series BT-</u> <u>3B</u>, 1999) indicates the elevation of the top of the bedrock surface in the immediate project area is between approximately 800 feet and 850 feet mean sea level (msl). Based on this mapping and the existing ground surface elevation between about 860 and 880 feet msl, the estimated depth to the top of bedrock surface may range from about 10 to 80 feet bgs. It should be noted that the referenced mapping utilizes 25-feet contours that are interpolated from topographic surface features and widely spaced data points where water wells and soil borings have encountered rock and therefore could have a significant elevation disparity within the project limits.

According to the mapping of bedrock geology in the area, (<u>Reconnaissance</u> <u>Bedrock Geology of the West Alexandria, Ohio Quadrangle</u>, *ODNR Geological Survey, Digital Map Series BG-2, 1999*), the surficial soil deposits on the site are underlain by Ordovician-age sedimentary rock identified as the Waynesville Formation. This formation consists of limestone and shale, averaging 70% shale and 30% limestone. The color is described as gray to bluish gray, weathering to light gray. The bedding is planar to irregular and thin to thick.

B. <u>Observations of the Project</u>

The site is located south of the existing West Alexandria Wastewater Treatment Plant which is located at the south end of Desota Drive in West Alexandria, Preble County, Ohio. The site is located in an agricultural field where at the time



of the field exploration the crops were harvested and remnants (stubble) of the crops remained.

The site has a high point at the site's southern boundary where a hilltop, with an elevation of about 890 feet, is located. From the hilltop at the southern boundary the site's existing grades slope downward to the north and east. At the northeast corner of the site where the existing wastewater treatment plant will connect to the proposed new treatment plant site, the ground surface slopes downward relatively steep to the northeast approximately with a topographic relief of about 20 feet in elevation.

Overhead utility lines were noted on the northeast corner of the site. According to the site pan a water line borders the northern property line and also is aligned along the northeast portion of the property. Manholes were noted within the existing treatment plant property, but there was no other evidence of underground or overhead utilities within the remainder of the project site.

C. <u>General Stratigraphy</u>

A general description of the subsurface materials encountered is presented below. Further details of the subsurface conditions encountered during CTL's geotechnical exploration are presented on the attached test boring records and soil profiles. Results of the soil laboratory tests are also attached.

1. Surficial Materials

The ground surface at each test boring location consisted of the native soils mixed with a small amount of organic material due to plowing of the agricultural field. The thickness of this plow zone was estimated at approximately 1 foot in the field, though organics/vegetative material (crop stubble remnants) were noted in the split spoon samples at a depth of 1.0-2.5 feet in test boring B-14-18.

2. Native Fine-Grained Soils

Beneath the surficial materials, the test borings generally encountered native fine grained (silt and clay) soils to depths ranging from 5.5 to 21.8 feet bgs. These materials were visually described as brown or gray, soft to hard, lean clay with varying amounts of sand and/or gravel, and sandy silty clay.

SPT N-values of the fine grained materials varied widely and ranged from 4 to 46 blows per foot (bpf), with an average value of about 14 bpf. The natural moisture content of these materials ranged from 8 to 28 percent, with an average of about 15 percent.

Six samples of the fine grained soils were tested in the laboratory for Atterberg Limits and particle size analysis. The results of these tests are presented in Appendix B and are summarized herein. The soils were



classified as sandy lean clay (CL) and sandy silty clay (CL-ML) according to the Unified Soil Classification System (USCS). These materials' Liquid Limits ranged from 21 to 42 percent, with Plasticity Indices ranging from 7 to 25 percent. An undisturbed tube sample obtained in boring B-08-18 at a depth of 5 to 7 feet had an unconfined compressive strength of 0.74 ksf with a moist unit weight of 124.1 pcf and a corresponding natural moisture content of 26.9 percent.

3. Native Coarse–Grained Soils

Coarse-grained (sand and gravel) soils were encountered beneath the finegrained materials in all test borings except B-10-18, B-16-18, and B-17-18. These native granular soils extended down to the planned boring termination depths. Test borings B-03-18, B-06-18, and B-15-18 also encountered a layer of granular soil that were encountered at the ground surface in addition to lower depths that that ranged from 5.5 to 8 feet bgs. The granular soils consisted of very loose to very dense, brown or gray, well-graded sand with gravel, well-graded sand with silt and gravel, wellgraded sand with silty clay and gravel, clayey sand, silty sand with gravel, silty clayey sand, and silty clayey sand with gravel. These materials were classified as SW, SW-SM, SW-SC, SC, SM, and SC-SM, according to the Unified Soil Classification System (USCS).

SPT N-values of the granular soils varied widely and ranged from 4 to 88 blows per foot (bpf) with an average of about 40 bpf. The natural moisture content of these soils ranged from 1 to 26 percent, with an average of about 8 percent.

4. Groundwater

The depth to groundwater was recorded both during drilling and at the completion of drilling activities. During drilling, groundwater was encountered in test borings B-02-18, B-04-18, B-05-18, B-06-18, B-08-18, and B-13-18 at depths ranging from 5.0 feet to 15.0 feet bgs (elevation 866.2 feet to 881.5 feet). At the completion of drilling, ground water was encountered in B-02-18, B-04-18, and B-08-18 at depths ranging from 8.0 feet to 12.0 feet bgs (elevation 872.9 feet to 878.8 feet). Table 3 provides detailed information on groundwater depths and corresponding elevations where encountered at the identified test boring locations.

Boring No.	Nearby Structure(s)	Depth of Structure, feet	Depth (Elevation) to Groundwater During Drilling, feet	Depth (Elevation) to Groundwater After Drilling, feet
B-02-18	Oxidation Ditch	10	5.0 (881.8)	8.0 (878.8)
B-04-18	Aerobic Digester	16	15.0 (871.8)	11.0 (875.8)

Table 3. Groundwater Depths and Elevations



Boring No.	Nearby Structure(s)	Depth of Structure, feet	Depth (Elevation) to Groundwater During Drilling, feet	Depth (Elevation) to Groundwater After Drilling, feet
	Tanks			
B-05-18	Clarifier Tanks/ UV Disinfection	19/ 8	13.5 (866.2)	N/A
B-06-18	Clarifier Tanks	19	5.0 (876.9)	N/A
B-08-18	Screen Building/ Oxidation Ditch	8/ 10	10.0 (874.9)	12.0 (872.9)
B-13-18	Oxidation Ditch	10	13.5 (869.4)	N/A

IV. DISCUSSION AND EVALUATION

Based on the bottom of structure/finish floor elevations previously presented in this report, the subsurface information collected from the test borings, laboratory testing, and our engineering analysis, the existing subsurface conditions are generally suitable for the proposed facility. The conditions which were encountered that pose a concern from a geotechnical and construction standpoint along with their implications are addressed below.

A. <u>Re-use of Excavated Materials as Engineered Fill</u>

CTL assumes that potential engineered fill to be used on this site will probably be from on-site excavated areas. If the on-site soils are to be utilized for engineered fill, they are generally suitable for reuse as structural fill, provided that they meet the requirements presented in this report. However, some of the fine-grained soils encountered at the locations of the proposed structures exhibit high moisture contents and will require drying before being used as engineered fill.

B. <u>Groundwater</u>

Based on our experience with the geology at this site, groundwater conditions affecting construction projects are related to trapped or perched water that may occur in irregular, discontinuous zones within the soil overburden, and may also be present at other elevations which were not identified on the test boring records at the time of the exploration. Based on the results of the test borings it appears groundwater bearing strata are present within 5 to 10 feet of the bearing elevations of the proposed structures near test borings B-02-18, B-04-18, B-08-18 and B-13-18.

When these water bearing strata (sand and/or gravel layers) are exposed in excavations (e.g. cut slopes, utility, or footing trenches) they can produce widely varying seepage durations and rates depending on recent rainfall activity and other hydrogeologic characteristics of the area. Therefore, groundwater levels may vary from those measured at the time of drilling and sampling as presented in



this report. If further determination of the site's ground water table and/or piezometric surface is necessary, additional data collection and evaluation by using monitoring wells and or piezometers is recommended.

V. <u>ANALYSIS AND RECOMMENDATIONS</u>

Based upon the preceding considerations as well as the subsurface information obtained from the field and laboratory testing and CTL's experience with these soil types, the following recommendations are provided. The design information provided by J&H provides a basis for CTL's recommendations, and has a direct impact on the recommendations presented. If changes to the design information presented in this report are made including construction sequencing/schedules, or additional information is available, CTL should be provided this information for our review, and if necessary, revised and/or additional recommendations can be provided.

A. Laboratory/Administrative Building

A finish floor elevation of 883 feet was assumed based on the existing ground surface elevations shown within the building footprint on the site plan. Approximately 1 to 2 feet of cut and fill will be required to achieve finish subgrade for the floor slab based on the approximate building footprint location. Assuming a bottom of footing elevation of 879 feet, the perimeter continuous wall footings will bear within the upper 3 to 5 feet below the existing ground surface. The materials encountered at the proposed foundation bearing elevation in borings B-09-18, B-14-18 and B-15-18 consist of stiff lean clays and loose clayey sands.

A spread foundation bearing directly on these native soils may be sized for a maximum net allowable foundation bearing pressure on the order of 2,000 pounds per square foot (psf). If a higher allowable bearing pressure is desired, it is recommended that the loose granular materials (encountered in B-15-18) be over-excavated in each column or wall spread footing down to an elevation of $875\pm$ feet to the underlying stiff lean clay material. The excavation should be backfilled up to the proposed finish subgrade elevation with lean concrete. However, it is anticipated that the upper loose granular soil may not allow for a stable, vertical sidewall footing excavation that can be readily backfilled. Therefore, a mass over-excavation of the entire building footprint may be required in order to facilitate the removal and subsequent placement of engineered fill to the required subgrade elevation. If the over-excavation and placement of engineered fill for backfill is performed, an allowable bearing capacity of 3,000 psf can be achieved. These bearing values would apply to the total design load.

B. <u>Aerobic Digesters</u>

The proposed facility plan shows two aerobic digesters being constructed with a future third aerobic digester planned to the immediate north of the first two structures. A bearing elevation of 870 feet was assumed for the aerobic digesters, based on a structure depth of 16 feet and an average existing ground surface



elevations of 886 feet. The materials encountered at the proposed bearing elevation in borings B-03-18, B-04-18, and B-09-18 consist of medium dense to very dense sands. A spread foundation bearing directly on these native soils may be sized for a maximum net allowable foundation bearing pressure of 4,000 pounds per square foot (psf). This bearing value would apply to the total design load.

C. <u>Screen/Grit Building</u>

A bearing elevation of 877 feet was assumed for the screen grit building, based on a structure depth of 8 feet and the existing ground surface elevation of 885 feet. The materials encountered at the proposed bearing elevation in boring B-08-18 consist of stiff to very stiff sandy lean clay. A spread foundation bearing directly on these native soils may be sized for a maximum net allowable foundation bearing pressure of 2,000 pounds per square foot (psf). This bearing value would apply to the total design load.

D. <u>Oxidation Ditches</u>

The proposed facility plan shows two oxidation ditches being constructed with a future third oxidation ditch planned to the immediate north of the first two structures. A bearing elevation of 874 feet was assumed for the oxidation ditches, based on a structure depth of 10 feet and the existing ground surface elevation of 884 feet. The materials encountered at or near the proposed bearing elevation in borings B-02-18, B-03-18, B-07-18, B-08-18, B-12-18, and B-13-18 consist of soft to very stiff sandy lean clay and sandy silty clay.

For the two proposed oxidation ditches where borings B-02-18, B-03-18, B-07-18 and B-08-18 are located, the recommended net allowable bearing capacity is 2,000 psf. For the future oxidation ditch soft compressible lean clay materials were encountered at the foundation bearing elevation in boring B-12-18 and B-13-18. These soils are not suitable for support of the structure. It is recommended that these materials be removed from beneath the proposed foundation bearing elevation down to an elevation of 865 feet. The excavation should be backfilled up to the proposed finish subgrade elevation with new compacted engineered fill. If this undercut is performed, an allowable bearing capacity of 3,000 psf can be achieved. This bearing value would apply to the total design load.

If the conditions at the proposed undercut elevation are not stable it may be necessary to stabilize the subgrade before placing engineered fill by drying and recompacting the material in place; placing a layer of biaxial geogrid followed by 12 inches of crushed granular material such as ODOT Item 304 or No. 57 sized gravel; or chemically stabilizing with lime or cement that meets ODOT requirements. Finish grade would then be re-established by using properly compacted, engineered soil fill. The building may then be supported by a mat foundation constructed into the newly placed, engineered fill.



E. <u>Clarifiers</u>

Bearing elevations ranging from 861.5 feet to 864.5 feet were assumed for the clarifiers, based on a structure depth of 19 feet and the existing ground surface elevation of 882 feet. The materials encountered at the proposed bearing elevations in borings B-01-18, B-06-18, and B-11-18 consist of dense to very dense sands. A spread foundation bearing directly on these native soils may be sized for a maximum net allowable foundation bearing pressure of 4,000 pounds per square foot (psf). This bearing value would apply to the total design load.

F. <u>Site Preparation and Earthwork Recommendations</u>

The following are general recommendations for site preparation. If it is anticipated that construction will occur at the time of year between October and May, the surficial soils are saturated and temperatures are not high enough to dry the soil expediently. Elevated soil moisture contents, for the soil types encountered, are not only difficult to reduce but also have a narrow range where they are suitable for compaction. These issues during the site preparation phase of construction should be taken into consideration when evaluating alternatives and the costs.

- 1. Strip topsoil, vegetation, and other organic materials or unsuitable materials from the construction area. These materials should be wasted from the site or they may be stockpiled for future use as topsoil or fill in landscape areas.
- 2. If chemical modification or stabilization is anticipated, based on the time of earthwork construction, a laboratory test program should be planned prior to construction to ensure proper type and amount of chemical additive is utilized for the soils. Usually the time frame for a laboratory testing program is about 4 to 6 weeks.
- 3. Maintain positive surface drainage to prevent water from ponding on the surface during construction and as part of final grading. Absorption of heavy rainfall, accumulations of water and heavy construction traffic may result in severely lowering the shear strength of the subgrade soils. If precipitation is expected, roll the fill surface with a rubber-tired or steel-drummed roller to improve surface runoff.
- 5. Contact the Geotechnical Engineer should the subgrade materials become excessively wet, dry, or frozen. If the construction schedule anticipates that earthwork and site work will be performed during typical wet weather months (October through May) the use of mechanical (geogrid and stone) or chemical stabilization is recommended to stabilize the subgrades for floor slabs and pavement and to maintain earthwork schedules. Chemical stabilization is the recommended method for stabilization for both short and long term subgrade support.



- 6. Engineered fill placement should extend beyond the limits of the proposed buildings and paved areas a minimum horizontal distance equal to the height of fill or 5 feet, whichever is greater.
- 7. Temporary excavations in excess of 4.0 feet in depth should be sloped or shored in accordance with OSHA regulations.

Due to the depths of some structures, CTL recommends that shoring be utilized along with a support or shield system as specified in OSHA Standard 1926 Subpart P App B.

Vertical trench walls and shoring systems should be designed by a licensed Professional Engineer, registered in the state of Ohio, familiar with the design of earth retention systems. The design should also take into account loading adjacent to the excavation such as foundation or vehicular loads and soil stockpiles. Lateral soil parameters for the design of trench walls and shoring systems are provided in Table 4 below.

	Material Type				
Soil Parameter	Off-site Clean Granular Engineered Fill	Clayey Sand/ Loose Sand	Lean Clay	Native Dense to Very Dense Sand	
Dry Unit Weight, pcf	125	120	120	130	
Saturated Unit Weight ¹ , pcf	145	140	140	150	
Moist Unit Weight, pcf	135	130	130	140	
Angle of Internal Friction, degrees	34	28	20	32	
At-Rest Pressure Coefficient, Ko	0.44	0.53	0.66	0.47	
Active Pressure Coefficient, Ka	0.28	0.36	0.49	0.31	
Passive Pressure Coefficient, K _p	3.54	2.77	2.04	3.25	

 Table 4. Soil Parameters for Lateral Earth Pressure

If groundwater is not drained, saturated or buoyant unit weights are recommended for design.

G. Engineered Fill Recommendations

1. Fill material required for this project may consist of the on-site excavated soils provided that they meet the requirements presented in this section. If grading plans do not provide adequate volumes of suitable excavated materials, borrow material will be required provided they meet the requirements of this report.



- 2. Limit the fill materials to a Liquid Limit less than 40, a Plasticity Index less than 20, a standard maximum dry density of at least 100 pcf (ASTM D698), a maximum particle size of 3 inches, and less than 3 percent by weight fibrous, organic matter.
- 3. New compacted engineered fill should be placed in layers not to exceed 8 inches in loose thickness, with each layer compacted to 100 percent of the maximum dry density as determined by ASTM D-698 standard method (AASHTO T-99), or as otherwise directed by the Geotechnical Engineer. The compacted fill should be placed with moisture content within the range of ± 3 percent of the Optimum Moisture Content.
- 4. CTL recommends field moisture-density tests be performed within the engineered fill for each lift of fill at a rate of at least one test for an area covering approximately every 10,000 square feet of engineered fill placed and compacted. A minimum of two field moisture-density tests should be performed per each entire lift of engineered fill placed and compacted.

Areas that do not meet the specified compaction criteria, based on the testing and observations of the engineering technician observing the earthwork activities and performing the field testing, should be reworked (scarified, moisture conditioned and re-compacted) to a suitable depth and re-tested. If the reworked engineered fill lift does not meet the earthwork specification the Geotechnical Engineer should be contacted to evaluate the current conditions and provide additional recommendations if necessary.

The observation and testing of engineered fill should be performed by qualified field personnel, performing the field density testing activities under the supervision of a registered professional engineer who specializes in geotechnical engineering, and is licensed in the State of Ohio.

H. <u>Slab on Grade Design Recommendations (Lab/Admin Building)</u>

- 1. CTL has assumed the effective modulus of subgrade reaction available for a suitably placed and compacted engineered fill soil consisting of lean clay (CL) materials is 150 pci.
- 2. CTL recommends that the slab on grade subgrade surface be observed and approved by the Geotechnical Engineer or his designated representative. If soft, loose, or highly plastic soils are encountered at the proposed subgrade level, these soils should be excavated and replaced with properly compacted engineered fill materials. The depth of the undercut will depend on the specific soil conditions observed by the Geotechnical Engineer or his designated representative.



- 3. Place a minimum 4-inch layer of clean, compacted gravel or crushed stone beneath the slab to enhance support and provide a working base. The actual thickness of the gravel layer should be based on slab design requirements.
- 4. Keep the crushed stone or gravel moist, but not wet, immediately prior to grade slab concrete placement to minimize curling of the slab due to differential curing conditions between the top and bottom of the slab.
- 5. Provide joints in the slabs around columns and along footing supported walls.

I. <u>General Building Foundation Support Recommendations</u>

- 1. CTL recommends that all bearing surfaces be observed and approved by the Geotechnical Engineer or his designated representative. If marginal soft to medium stiff, loose, or highly plastic soils are encountered these soils should be undercut and removed and lean concrete placed up to the proposed footing bearing elevation.
- 2. The removal of soil for the construction of the underground structures (oxidation ditch, screen building, aerobic digester tanks, clarifier tanks, and UV disinfection) will result in a net reduction of overburden pressure at the structures' bearing elevations. CTL has determined that the anticipated loads provided by these structures will not increase the bearing pressure to a value higher than what is currently applied by the native soil. Therefore, a potential buoyant condition may occur if the structures are not designed for the case when the groundwater elevation outside the structures is significantly higher relative to the water level within the structures. Therefore, it is recommended that the structures be designed with a dead load that is sufficient to offset buoyant forces. Additional alternatives to resist uplifting forces include 1) anchors or 2) design an active pumping and/or passive system that would lower the surrounding ground water elevation when water levels within the structures are lowered for maintenance or other similar conditions.
- 3. In general, the anticipated settlements (total and differential) as a result of the above recommended foundation pressures should be within tolerable limits (1 inch total and ½ inch differential, respectively) for a masonry-framed building or a concrete reinforced structure, assuming the foundation soil improvement recommendations in this report are followed.
- 4. Minimum widths for individual columns and continuous wall footings should be 24 and 18 inches, respectively. Minimum widths are considered advisable to provide a margin of safety against local or punching shear failure.



- 5. Exterior footings should be constructed at a minimum depth of 36 inches below the lowest adjacent exterior grade to offset the effects of frost penetration. Interior footings in areas of controlled temperature may be constructed at shallower depths below the floor slab provided that the soils supporting the footings exhibit sufficient shear strength for supporting the foundation contact.
- 6. Protect foundation support materials exposed in open excavations from freezing weather, severe drying, and water accumulation.
- 7. Remove any soils that become unsuitable due to exposure prior to concrete placement.
- 8. Excavate only the foundations or bottom of structures that can be placed with concrete the same day. Otherwise place a "lean" concrete mud-mat over the bearing soils if the excavations must remain open overnight or for an extended period of time.
- 9. Foundation concrete should completely fill the opened excavation. Forming the foundations and then backfilling the space behind the forms tends to allow moisture to penetrate and soften bearing level materials which may result in poor foundation performance.

J. <u>General Groundwater Control Recommendations</u>

It is imperative that a comprehensive groundwater control plan be developed for the underground structures.

Typically, short-term groundwater control required during construction is addressed by dewatering methods utilized to perform construction in the "dry". The methods typically employed for construction in the dry depend on various hydrogeological factors in addition to other factors, including but not limited to:

- recent precipitation,
- the depth of construction,
- duration of the construction,
- the proximity of other proposed structures both in plan location and bottom of structure elevation,
- construction methods.

It is recommended that the dewatering plan be coordinated with the anticipated stage of construction for the structures. If dewatering is achieved by lowering the groundwater elevation, the lowest elevation should be performed initially, in order to minimize the potential settlement from dewatering.

For groundwater encountered at shallower elevations sump and pump methods are typically suitable for relative short term durations. For long term dewatering and/or deeper excavations; 1) well points (vacuum) employed at multiple



elevation stages; or 2) cutoff walls (e.g. soil-bentonite slurry, cement-bentonite slurry, tangent or secant drilled shaft walls, steel sheet piling, etc.) may be more appropriate. The design of a dewatering system is beyond the scope of this exploration. These approaches can be further addressed once details of the facility design are developed.

K. <u>Pavements</u>

The proposed subgrade elevations in the pavement areas are generally within ± 1 foot of the existing ground surface elevations, however the proposed subgrade elevations in the northeast corner of the site were not provided.

- 1. Subgrade of paved areas should be observed and approved by the Soil Engineer. Soils with a maximum dry weight of less than 100 pounds per cubic foot (pcf) are unsuitable for use in the upper 12 inches of subgrade. Such soils should be replaced with other suitable soils or granular material.
- 2. The test borings encountered medium stiff to stiff sandy lean clay or loose clayey sand materials at the ground surface. Some of these soils exhibited moisture contents above the optimum value for these soil types. The use of chemical stabilization with lime or Portland cement is recommended in order to stabilize the subgrade and prevent pavement failure due to vertical movement of the subgrade soils. The depth of the stabilization should be a minimum of 14 inches below the planned top of subgrade elevation. For the purpose of a preliminary cost estimate, the amount of lime or cement used for soil modification may be assumed to be about 6 percent by weight. Laboratory testing in accordance with ODOT Item 206 will be required to determine the recommended type of chemical modifier and the amount of chemical modifier to be added to the soil. This testing should be performed by a qualified AMRL accredited laboratory prior to performing the stabilization.
- 3. Subsequent to site clearing and chemical stabilization and prior to any fill or aggregate placement, all exposed surfaces should be proofrolled with an approved 25-ton loaded, tandem axle truck to verify that a relatively unyielding surface is achieved. Soft or loose soils, if encountered, should be disked, dried and recompacted or undercut and replaced with compacted engineered fill or otherwise as directed by the Geotechnical Engineer.
- 4. In the event that excessive rutting or deflections occur during proofrolling operations, yielding soils should be addressed as noted in the preceding *Site Preparation and Earthwork Recommendations* section of this report.
- 5. Near surface soils are predominantly cohesive and will be affected by the moisture content of the soils. Therefore, it is highly recommended that any surface and subsurface water be permanently and quickly drained from the



area to limit the weakening of the subgrade soil used for pavement support. Without drainage, any modification/stabilization procedure undertaken should be considered temporary. It is recommended that a drainage system be designed to permanently dewater the subbase aggregate and associated subgrade soils into the site's storm sewer system or away from any building and pavements. Finger drains should be installed in the area of catch basins.

L. <u>Seismic Site Class Recommendation</u>

CTL recommends the subject property be assigned a seismic site class of D in accordance with the 2011 Ohio Building Code.

VI. <u>CHANGED CONDITIONS</u>

The evaluations, conclusions, and recommendations in this report are based on our interpretation of the field and laboratory data obtained during the exploration, our understanding of the project and our experience with similar sites and subsurface conditions using generally accepted geotechnical engineering practices. Although individual test borings are representative of the subsurface conditions at the boring locations on the dates drilled, they are not necessarily representative of the subsurface conditions between boring locations or subsurface conditions during other seasons of the year.

In the event that changes in the project are proposed, additional information becomes available, or if it is apparent that subsurface conditions are different from those provided in this report, CTL should be notified so that our recommendations can be modified, if required.

VII. <u>TESTING AND OBSERVATION</u>

During the design process, it is recommended that CTL work with the project designers to confirm that the geotechnical recommendations are properly incorporated into the final plans and specifications, and to assist with establishing criteria for the construction observation and testing.

CTL is not responsible for independent conclusions, opinions and recommendations made by others based on the data and recommendations provided in this report. It is recommended that CTL be retained to provide construction quality control services on this project. If CTL is not retained for these services, CTL shall assume no responsibility for compliance with the design concepts or recommendations provided.



VIII. <u>CLOSING</u>

The report was prepared by CTL Engineering, Inc. (Consultant) solely for the use of The Village of West Alexandria (Client) in accordance with an executed contract. The Client's use of or reliance on this report is limited by the terms and conditions of the contract and by the qualifications and limitations stated in the report. It is also acknowledged that the Client's use of and reliance of this report is limited for reasons which include: actual site conditions that may change with time; hidden conditions, not discoverable within the scope of the assessment, may exist at the site; and the scope of the investigation may have been limited by time, budget and other constraints imposed by the Client.

Neither the report, nor its contents, conclusions or recommendations, are intended for the use of any party other than the Client. Consultant and the Client assume no liability for any reliance placed on this report by such party. The rights of the Client under contract may not be assigned to any person or entity, without the consent of the Consultant which consent shall not be unreasonably withheld.

This geotechnical report does not address the environmental conditions of the site. The Consultant is not responsible for consequences or conditions arising from facts that were concealed, withheld, or not fully disclosed at the time the assessment was conducted.

To the fullest extent permitted by law, the Consultant and Client agree to indemnify and hold each other, and their officers and employees harmless from and against claims, damages, losses and expenses arising out of unknown or concealed conditions. Furthermore, neither the Consultant nor its employees shall be liable to the Owner in an amount in excess of the available professional liability insurance coverage of the Consultant. In addition, Client and Consultant agree neither shall be liable for any special, indirect or consequential damages of any kind or nature.

The Consultant's services have been provided consistent with its professional standard of care. No other warranties are made, either expressed or implied.

Respectfully Submitted,

CTL ENGINEERING, INC.

Josh C. Williams Project Engineer

Uny R Bath

Doug R. Batt, P.E. Project Engineer License No. E-58801

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APPENDIX A

TEST BORING RECORDS



EXPLANATION OF TERMS AND SOIL DESCRIPTIONS (ASTM D2487 & ASTM D2488)

Consistency and Relative Density Descriptions

Descriptors for soil consistency used in this report are based upon the Standard Penetration Test (SPT), ASTM D 1587, with the penetration (N) values corrected to N_{60} , based upon the efficiency of the SPT Hammer (Energy Ratio) used for the soil sampling.

<u>NON-</u> [GW, GP, G	<u>COHESIVE SOILS</u> GM, GC, SW, SP, SN	<u>5</u> 4, SC]		<u>COHESIVE SOILS</u> [ML, MH, CL, CH]	
<u>Relative Density</u> <u>or Consistency</u>	<u>SPT-N60</u> (blows/foot, bpf)	<u>Suitability</u>	<u>Stiffness or</u> Consistency	<u>SPT-N₆₀ (blows/foot, bpf)</u>	<u>Suitability</u>
Very Loose	0 - 4	Poor	Very Soft	0 - 1	Very Poor
Loose	5 - 10	Marginal	Soft	2 - 4	Poor
Medium Dense	11 - 30	Satisfactory	Medium Stiff	5 - 8	Marginal
Dense	31 - 50	Good	Stiff	9-15	Satisfactory
Very Dense	Over 50	Very Good	Very Stiff	16 - 30	Good
			Hard	Over 30	Very Good

COMPONENT MODIFIERS

<u>AST</u> (Visua	<u>M D2488</u> Il-Manual)	<u>ASTM I</u> (USC	Organic Soils		
Modifier	% by Weight	Modifier	% by Weight	Modifier	% by Weight
Trace of	0 - 1	with sand or gravel	15 - 29	Highly	> 10
Traces of	2 - 10	Sandy or Gravelly	\geq 30	Moderately	4 - 10
Little	11 - 20	with silt or clay	5 - 12	Slightly	2 - 4
Some	21 - 35	Silty or Clayey	> 12	Inorganic	< 2
"And"	36 - 50	Organic	$LL_{oven}/LL_{air} < 0.75$		

MOISTURE DESCRIPTIONS

Terms	<u>Non-Cohesive Soils</u>	Cohesive Soils	<u>Suitability</u>
Dry	Moisture Absent	Powdery	Marginal
Damp	Some Moisture	Below Plastic Limit	Good
Moist	Damp to the Touch	Between Plastic and Liquid Limits	Marginal
Wet	Visible Water	Above Liquid Limit	Poor
		-	

PARTICLE SIZE DESCRIPTIONS

.

<u>Component</u>	USCS Particle Size
Boulders	≥ 12-in. (300 mm)
Cobbles	< 12-in. (300 mm) to 3-in. (75 mm)
Coarse Gravel	< 3-in. (75 mm) to 3/4-in. (19.05 mm)
Fine Gravel	< 3/4-in. 19.05 mm) to #4 Sieve (4.75 mm)
Coarse Sand	< #4 Sieve (4.75 mm) to #10 Sieve (2.00 mm)
Medium Sand	< #10 Sieve (2.00 mm) to #40 Sieve (0.425 mm)
Fine Sand	< #40 Sieve (0.425 mm) to #200 Sieve (0.074 mm)
Silt	< #200 Sieve (0.074 mm) to 0.005 mm
Clay	< 0.005 mm

SOIL DESC	RIPTIONS BA	SED ON THE	UNIFIED SOIL	CLASSIFICAT	ION SYSTEM (ASTM D 2487)
	Major Division		Group Symbol	Letter Symbol	Group Name*
		Gravel with <		GW	Well Graded GRAVEL
		5% Fines	0	GP	Poorly Graded GRAVEL
	GRAVEL -	Gravel with		GW-GM	Well Graded GRAVEL with silt
	Percent	Between 5		GW-GC	Well Graded Gravel with clay
	percent	and 15%	0000000	GP-GM	Poorly Graded GRAVEL with silt
	SAND	Fines		GP-GC	Poorly Graded GRAVEL with clay
Coarse		Gravel with S		GM	Silty GRAVEL
Less Than 50		15% Fines		GC	Clayey GRAVEL
Percent				GC-GM	Silty, Clayey GRAVEL
Passing the # 200 Sieve		Sand with <		SW	Well Graded SAND
		5% Fines		SP	Poorly Graded SAND
	SAND -			SW-SM	Well Graded SAND with silt
	Percent	Between 5		SW-SC	Well Graded SAND with clay
	SAND≥ percent	and 15%		SP-SM	Poorly Graded SAND with silt
	GRAVEL	Fines		SP-SC	Poorly Graded SAND with clay
				SM	Silty SAND
		Sand with ≥		SC	Clayey SAND
		1370 1 11/23		SC-SM	Silty, Clayey SAND
				ML	SILT
Fine Grained		Liquid Limit		CL	Lean CLAY
50 percent or		Less Than 50		CL-ML	SILTY CLAY
more Passing	SILT and CLAY			OL	Organic SILT, CLAY, or SILTY CLAY
Sieve			///////////////////////////////////////	СН	Fat CLAY
		Liquid Limit		МН	Elastic SILT
				ОН	Organic SILT or CLAY
Hig	hly Organic Soil	S		PT	Peat/Marl
	Coarse	with sil	t or clay	5 to	12 % Silt or Clay by weight
* Additional	Grained Soils	Silty o	r Clayey	more th	an 12 % Silt or Clay by weight
Modifiers	Fine Grained	with sand	d or gravel	15 to 29	9 % Sand or Gravel by weight
	Soils	Sandy o	r Gravelly	30 % or r	nore Sand or Gravel by weight
	Ranne of Plasticity	ι	JSCS PLASTICITY C	HART	
	60 Low /	Slight	Moderate	High	Very High Extreme
	For classification of	fine-grained soils and fine-g	rained fraction	UNE	Extremely
	50 Equation of "A" Line	2 2			
	40	5 LL-25.5 then FI-0.75(LL-20)		·	"A" UNE
DEX (PI)	Vertical at LL=16 to	e PI=7 then PI=0.9(LL-8)	CH or 0	он	
	30		1	Marginal	
PLASTIC	20			Soils	
	20	CL or (DL	MH or OH	Desformed fing grain - d11 in
	10	· · /			inorganic and lies below "U" Line and left of LL=50
	4	CL-ML ML or	OL		(CL / ML Soils)

Good Soils

LIQUID LIMIT (II)

			TE	ST E	ORI	NG	REC	ORD								
CLIEN.	т	: Village We	st Alexandria						_		BO	RING NC	D.:	B-0 1	-18	
PROJE	ECT	: West Alexa	andria WWTP						_		SHI	EET	1	0	F	2
LOCAT	ΓΙΟΝ	: 33 Desoto	Drive						_		DA	TE STAR	RTED	: 03-2	28-18	
PROJE	ECT NO.	: 180500060	CIN	-							DA	TE COM	PLETED	: 03-2	28-18	
BORIN	IG ELE	VATION	: 883.1 Feet	RIG	ΓΥΡΕ		: CME	45				ILLER	:_[DS		
	NOR	THING	: 640982.8613	CASI	NG DIA	۱.	: 3.25"					MPERAT	URE : 4	10s		
	EAS	TING	: 1399179.0976	COR	E SIZE		: N/A				WE	ATHER	:_(Cloudy		
	DEP	тн	: 30.0 Feet	HAM	MER		: Auto				-					
	BOR	ING METHO	D: HSA	ENE	RGY RA	TIO	: 84.1									
GROU	NDWATE	ER: End	ountered at None At co	ompletic	n <u>Dry</u>		1		1	1						
STRATUM ELEVATION	SAMPLE DEPTH	c	OII /MATERIAL DESCRIPTI	N		STRATUM DEPTH	SAMPLE NUMBER	SPT per 6"	N ₆₀	RECOVERY (%)	MOISTURE	TOTAL UNIT WEIGHT Pcf	UNCONF. COMP., ksf		ERBE LIMITS	ERG
							SS-1	3 4 5	13	100	16		3.5*	28	15	13
	5	Stiff to Very (CL) , Damp	Stiff, Brown SANDY LEAN C to Moist	LAY			SS-2	4 4 6	14	100	15		4.5*			
							SS-3	4 6 8	20	100	8		5.0*			
872.6_	10					_10.5	SS-4	4 5 8	18	100	10		7.0*			
870.1_		Very Stiff, G Damp (TILL	iray SANDY LEAN CLAY (CL))	,		_13.0	SS-5	5 10 11	29	67	9		9.0*			
866.3	-	Dense, Brov GRAVEL ar	wn WELL GRADED SAND wit d SILTY CLAY (SW-SC), Moi	h st		16.8	SS-6	10 15 20	49	56	8					
	20	Very Dense GRAVEL ar	, Gray WELL GRADED SANE d SILTY CLAY (SW-SC), Dar <u>Continued on n</u> ext page	with np			SS-7	18 20 22	59	67	5					
		2105 Sc	happelle Lane	E		METHO			NG ME	THOD		A		TION	3	
	TL ering 2	Cincinna Telepho Fax: 51 Email:	ati, Ohio 45240 one: 513-722-8665 3-834-6650 ctlcin@ctleng.com	HSA- SFA- RC - MD - WD - HA -	Hollow Solid F Rock C Mud Di Wash I Hand A	Stem A light Au coring filling Drilling Luger	liger SS Iger ST CF BS	o - Split ∜ ⁻ - Shelb R - Rock S - Bag S	Spoon y Tube Core S Sample	Samp e Sam Sample e	ie * ple LL e PL PI SF	- Har Liqu - Liqu - Plas - Plas - Stat - Stat	nd Penetr uid Limit stic Limit sticity Inc ndard Pe ndard Pe	lex netrati	on Te on	st

		TEST B	BORI	NG	REC	ORD								
CLIEN	T	: Village West Alexandria					-		BOI	RING NC).:	B-0 1	-18	
PROJE		: West Alexandria WWTP							SHE	ET	2	0	F :	2
STRATUM ELEVATION	SAMPLE	SOIL/MATERIAL DESCRIPTION	·.·//	STRATUM DEPTH	SAMPLE NUMBER	SPT per 6"	N ₆₀	RECOVERY (%)	MOISTURE	TOTAL UNIT WEIGHT pcf	UNCONF. COMP., ksf	AT		RG PI
	25_/	Very Dense, Gray WELL GRADED SAND with GRAVEL and SILTY CLAY (SW-SC), Damp			SS-8	20 25 30	77	100	6					
853.1_	30_	BOTTOM OF BORING		30.0	SS-9	23 26 25	71	56	6					
	40_													
	45_													
		2105 Schappelle LaneHSA-Cincinnati, Ohio 45240SFA-Telephone: 513-722-8665RC -Fax: 513-834-6650WD -Email: ctlcin@ctleng.comHA -	BORING Hollow Solid F Rock C Mud Dr Wash I Hand A	METHO Stem A light Au Coring rilling Drilling Auger	JD S uger SS ger ST CI BS	SAMPLIN S - Split S C - Shelb R - Rock S - Bag S	IG ME Spoon y Tube Core s ample	Samp Samp Sample	le * ple LL e PL PI SF N6	Al - Har - Liqu - Plas - Plas 2T - Stal 50 - Stal prmalized	BBREVIA ad Penetri aid Limit stic Limit sticity Ind ndard Pe ndard Pe I to 60%	internat Detrat	ion Te:	st

			TE	ST B	ORI	NG	REC	ORD								
CLIEN	т	: Village	West Alexandria						_		BOI	RING NO	D.:	B-02	-18	
PROJE	СТ	: West A	Alexandria WWTP						_		SHE	EET	1	0	F	2
LOCAT	TION	: 33 Des	soto Drive						_		DA	TE STAF	RTED	: 03-2	8-18	
PROJE	ECT NO). : 18050	006CIN								DA	ГЕ СОМ	PLETED	: 03-2	8-18	
BORIN	IG EL	EVATION	: 886.8 Feet	_ RIG 1	YPE		: CME	45			DRI	LLER	:_0	DS		
	NC	RTHING	: 640984.1213	CASI	NG DIA	۱.	: 3.25"				TEN	IPERAT	URE: 4	l0s		
	EA	STING	: 1399104.1082	COR	E SIZE		: N/A				WE	ATHER	: 0	Cloudy		
	DE	PTH	: 35.0 Feet	HAMI	MER		: Auto				-					
	BC	RING MET	THOD: HSA		RGY RA		: 84.1				-					
GROU	NDWA	TER: 工	Encountered at <u>5.0'</u> Σ At c	completio	n <u>8.0'</u>	1	1				1			1		
ATION	귀표					H ⁻ H	ole Ber			OVERY	TURE	AL UNIT SHT	DNF. P., ksf	ATT L	ERBE	ERG
STRA ELEV	SAMF		SOIL/MATERIAL DESCRIPT	ION		STRA DEP1	SAMF NUMF	SPT per 6	N ₆₀	RECO (%)	MOIS	TOTA WEIG pcf	COMI	LL	PL	PI
883.8_		Medium (CL), W	a Stiff, Brown SANDY LEAN CLA et	Y		3.0	SS-1	2 3 3	8	100	17					
Ţ	_ 						SS-2	2 3 4	10	100	13		2.0*			
Ţ	- - 	Stiff to V (CL), W	√ery Stiff, Brown SANDY LEAN C et (TILL)	CLAY			SS-3	2 3 5	11	100	12		4.5*			
876.3_	10_					10.5	SS-4	4 5 8	18	100	12		5.0*			
873.8_		Soft, Gr (TILL)	ay LEAN CLAY with SAND (CL)	, Wet		13.0	SS-5	3 1 2	4	100	17		2.5*			
8700	15_/	Medium GRAVE	n Stiff, Gray SANDY LEAN CLAY L (CL), Moist	with		16.9	SS-6	3 3 3	8	56	10		2.0*			
	20_	Hard, G (CL), M	iray SANDY LEAN CLAY with GF oist Continued on next page	RAVEL		10.0	SS-7	15 16 17	46	67	10		9.0*			
		2105	Schappelle Lane	B	ORING	METH	DD S	SAMPLI	NG ME	THOD		A	BBREVIA	TIONS	\$	
	T L ERING ≌	Cinc Tele Fax: Ema	innati, Ohio 45240 phone: 513-722-8665 513-834-6650 il: ctlcin@ctleng.com	HSA- SFA- RC - MD - WD - HA -	Hollow Solid F Rock C Mud Dr Wash I Hand A	Stem A light Au Coring rilling Drilling Nuger	Auger SS Iger ST CF BS	5 - Split 5 - Shelb R - Rock 5 - Bag S	Spoon y Tube Core S ample	Samp e Sam Sample e	le * ple LL e PL PI SF N6	- Har - Liqu - Plas - Plas - Plas - Sta - Sta	nd Penetr uid Limit stic Limit sticity Ind ndard Pe ndard Pe	omete lex netrati netrati	r on Te on	st

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STF ELE	SAN	SOIL/MATERIAL DESCRIPTION	V/////	STF	SAN	SPT	N ₆₀	RE(%)	0 V O V O	p KD Pof	CO	LL	PL	ΡI
865.0_	-	Hard, Gray SANDY LEAN CLAY with GRAV (CL), Moist	EL	_21.8										
	25_				SS-8	18 19 25	62	56	5					
	30	Dense to Very Dense, Brown WELL GRADE SAND with GRAVEL and SILTY CLAY (SW-SC), Moist	D		SS-9	18 15 13	39	56	5					
851.8_	35	BOTTOM OF BORING		35.0	SS-10	14 16 20	50	67	5					
	40													
	45_													
ENGINEE	TL ERING ^w	2105 Schappelle Lane Cincinnati, Ohio 45240 Telephone: 513-722-8665 Fax: 513-834-6650 Email: ctlcin@ctleng.com	BORING HSA-Hollow SFA-Solid Fl RC -Rock C MD -Mud Dr MD -Wash I HA -Hand A	METHO Stem A light Au oring illing Drilling uger	DD SA Auger SS Iger ST CR BS	AMPLIN - Split S - Shelby - Rock (- Bag S	IG ME poon / Tube Core S ample	THOD Sample Sample	le * ole LL e PL PI SF N6 No	Al - Har - Liqu - Plas - Plas 2T - Star 0 - Star 0 - Star	BBREVIA ad Penetr uid Limit stic Limit sticity Ind ndard Pe ndard Pe I to 60%	ex netrati Drill R	s ion Tea ion od ER	st

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PROJE	ECT	: West Alex	andria WWTP								SHI	EET	1	0	F	2
LOCAT	TION	: 33 Desoto	Drive						_		DA	TE STAF	RTED	: 03-2	28-18	
PROJE	ECT NO.	: 18050006	CIN						-		DA	TE COM	PLETED	: 03-2	28-18	
BORIN	G ELE	VATION	: 887.6 Feet	RIG T	YPE		: CME	45			DR	ILLER	: [DS		
	NOR	THING	: 640985.3813	CASI	NG DIA	۱.	: 3.25"					MPERAT	URE : 4	10s		
	EAS	TING	: 1399029.1188	CORE	E SIZE		: N/A				WE	ATHER	: (Cloudy		
	DEP	ТН	: 35.0 Feet	HAMN	ИER		: Auto				-		_			
	BOR	ING METHO	D: HSA		RGY RA	OIT	: 84.1				-					
GROU	NDWATE	ER: End	countered at <u>None</u> At co	mpletio	n <u>Dry</u>											
ATUM VATION	IPLE TH					ATUM TH	IPLE 1BER			OVERY	STURE	AL UNIT GHT	:ONF. 1P., ksf	ATT I	ERBE	ERG S
STR ELE	SAM DEP	S	SOIL/MATERIAL DESCRIPTIC	N		STR DEP	SAM NUN	SPT per 6	N ₆₀	REC (%)	NON CON	TOT WEI	CON CON	LL	PL	PI
		Loose to M SAND (SC)	edium Dense, Brown CLAYEY , Wet	,			SS-1	3 3 2 3	7	100	15		3.0*	22	14	8
882.1_	5					_5.5	SS-2	35	11	100	13		4.5*			
	-/						SS-3	3 3 6	13	67	10		4.0*			
	10						SS-4	3 5 5	14	100	9		6.0*			
		Stiff to Very (CL), Wet (/ Stiff, Gray SANDY LEAN CL/ TILL)	ΑY			SS-5	3 5 3	11	89	19		3.0*			
741E-1901 9/10/10 870.8	15					16.8	SS-6	3 7 5	17	100	12		5.0*			
רעסרד גיטאיז ע וו גיטאיז 1805טטטטטעטעטעט גע איז גערערד געסעד	20	Medium De with GRAV	ense, Gray SILTY CLAYEY SA EL (SC-SM), Wet Continued on next page	ND			SS-7	5 6 8	20	100	10		5.5*	18	13	5
		2105 S	chappelle Lane	В	ORING	METHO	DD S	AMPLI	NG ME	THOD		Α	BBREVIA	TIONS	5	
	TL ering ^g	Cincinn Telepho Fax: 57 Email:	ati, Ohio 45240 one: 513-722-8665 13-834-6650 ctlcin@ctleng.com	HSA- SFA- RC - MD - WD - HA -	Hollow Solid F Rock C Mud Dr Wash [Hand A	Stem A light Au coring rilling Drilling Luger	Auger SS Iger ST CF BS	5 - Split 5 - Shelb R - Rock 5 - Bag S	Spoon y Tube Core S Sample	Samp Sample Sample	le * ple LL e PL PI SF	- Har - Liqu - Plas - Plas - Plas - Sta - Sta	nd Peneti uid Limit stic Limit sticity Inc ndard Pe ndard Pe	romete lex enetrati	on Te	st

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PROJE									SHE		2	0		2
RATUM EVATION	MPLE PTH			RATUM PTH	MPLE MBER	- ¹ 9	0	COVERY	ISTURE	TAL UNIT IGHT	CONF. MP., ksf	AT1 I	ERBE	RG
STI ELE	SAI	SOIL/MATERIAL DESCRIPTION	N	STI DE	SAI NU	SP.	N ₆₍	RĒ (%	о М О О О О	p ME	NO	LL	PL	ΡI
865.8	-	Medium Dense, Gray SILTY CLAYEY SAN with GRAVEL (SC-SM), Wet	D	21.8										
	25				SS-8	15 20 22	59	56	7					
	30	Very Dense, Brown WELL GRADED SAND with GRAVEL and SILTY CLAY (SW-SC), Moist			SS-9	15 28 35	88	56	4					
852.6_	35	BOTTOM OF BORING		_35.0	SS-10	18 23 27	70	67	6					
	40													
	45													
ENGINEE	TL ERING É	2105 Schappelle Lane Cincinnati, Ohio 45240 Telephone: 513-722-8665 Fax: 513-834-6650 Email: ctlcin@ctleng.com	BORING HSA-Hollow SFA-Solid Fl RC -Rock C MD -Mud Dr WD -Wash E HA -Hand A	METHO Stem A ight Au oring illing Drilling uger	DD S Juger SS ger ST CR BS	AMPLIN - Split S - Shelby - Rock (- Bag S	i G ME poon / Tube Core S ample	THOD Sample Sample	e * ole LL PL PI SF N6 N0	At - Han - Liqu - Plas - Plas 2T - Star 0 - Star mmalized	BBREVIA ad Penetr id Limit stic Limit sticity Ind ndard Pe ndard Pe to 60%	romete lex netrati Drill R	s ion Tea ion od ER	st

			TE	ST B	ORI	NG	REC	ORD								
CLIEN	т	: Village We	est Alexandria						_		BOI	RING NO	D.:	B-04	-18	
PROJE	СТ	: West Alexa	andria WWTP						_		SHE	EET	1	0	=:	2
LOCAT	ION	: 33 Desoto	Drive						_		DA	TE STAR	RTED	: 03-2	8-18	
PROJE	ECT NC). : 180500060	CIN								DA	LE COM	PLETED	: 03-2	8-18	
BORIN	G EL	EVATION	: 886.8 Feet	RIG T	YPE		: CME	45			DRI	LLER	: <u> </u>	os		
	NC	RTHING	: 640986.6413	CASI	NG DIA	۱.	: 3.25"					IPERAT	URE : _4	0s		
	EA	STING	: 1398954.1294	CORE	E SIZE		: N/A				WE	ATHER	:_0	Cloudy		
	DE	PTH	: 35.0 Feet	HAM	MER		: Auto									
	BC	RING METHO	D: HSA	ENER	RGY RA	TIO	: 84.1									
GROU	NDWA	TER: I Enc	countered at <u>15.0'</u> Σ At co	mpletio	n <u>11.0'</u>				1		1					
ΣZ						5				Ϋ́	₩⊢	μ	.st	ATT	ERBE	RG
ATIO	귀도					N L	CLE BER			N		Б Н Н	ONF k	L	IMITS	3
LEV	AMF					EPT	AMF	PT er 6"	09	Щ Ш Э	SIO	1 EIGA	OMI			
Ξω	0 U	5	SOIL/MATERIAL DESCRIPTIO	DN		D N D	νz	୍ ତ ଜୁ	Z	R ©	Συ	≓≥ă	⊃U	LL	PL	PI
		Stiff Brown	SANDY I FAN CLAY (CL) MC	nist				3								
	-/						SS-1	3	10	100	23		3.5*			
883.8		-				3.0		-								
-																
	-						SS-2	3	11	100	12		6.0*			
	5_/	N					002	5			12		0.0			
	+							4								
		Medium Stil	ff to Stiff, Brown SANDY LEAN	1			SS-3	4	13	100	16		2.0*			
	17							5								
	-															
		7						3								
							SS-4	3	8	89	14		3.0*			
876 3	10_/					10.5		3								
	z 1					10.0										
		Λ					оо г	3	10	100			C 0*			
	-/	N					55-5	4	13	100			6.0*			
		Stiff to Very	Stiff, Gray SANDY LEAN CLA	AY												
<u>•</u>	-\	(CL) , Wet (1	FILL)				SS-6	5	18	100	10		6.0*			
	15_							8								
3																
	-															
5 870.0_						16.8										
5																
5	-	Very Dense	, Brown WELL GRADED SAN	D												
5	1	with GRAVI	EL and SILTY CLAY (SW-SC),					20								
	20						SS-7	25	70	67	4					
NOPEO L	20	1														
°			Continued on next page		1.º.¥.¥.											
		2105 Sc	chappelle Lane	HSA-	Hollow	Stem 4		S-Split S	NG ME Spoon	Samp	le *	Al - Har	d Penetr	omete	> r	
Γ.		Cincinn	ati, Ohio 45240	SFA-	Solid F	light Au	iger ST	-Shelb	y Tub	Sam	ple LL	- Liqu	uid Limit			
	TL	Telepho	one: 513-722-8665	RC -		oring	CF	R-Rock	Core Sample	Sample	e PL	- Plas	stic Limit	ev		
	ERING 🖻	Fax: 51	3-834-6650	WD -	Wash [Drilling	DC	, - bay с	ampie	•	SF	PT - Sta	ndard Pe	netrati	on Te	st
		Email:	ctlcin@ctleng.com	HA -	Hand A	uger					Ne	0 - Sta	ndard Pe	netrati	on	
-												nnalizeo	i lu bU% l	א ווויט Re	Ju ER	

		TEST	BORI	NG	RECO	ORD								
CLIEN	т	: Village West Alexandria					-		BO	RING NC).:	B-0 4	-18	
PROJE		: West Alexandria WWTP			[1	1	SHE	EET	2	O	F :	2
STRATUM ELEVATION	SAMPLE DEPTH	SOIL/MATERIAL DESCRIPTION		STRATUM DEPTH	SAMPLE NUMBER	SPT per 6"	N ₆₀	RECOVERY (%)	MOISTURE CONTENT	TOTAL UNIT WEIGHT pcf	UNCONF. COMP., ksf	ATT L	ERBE IMITS PL	RG
860.0_		Very Dense, Brown WELL GRADED SAND with GRAVEL and SILTY CLAY (SW-SC), Damp		26.8	SS-8	15 20 19	55	56	5					
	30	Very Dense, Gray WELL GRADED SAND with GRAVEL and SILTY CLAY (SW-SC), Damp			SS-9	15 25 20	63	67	5					
851.8_	35	BOTTOM OF BORING		35.0	SS-10	18 20 22	59	67	6					
	- - 40_ - -													
	45_													
	TL ering 2	2105 Schappelle Lane Cincinnati, Ohio 45240 Telephone: 513-722-8665 Fax: 513-834-6650 Email: ctlcin@ctleng.com	BORING A-Hollow A-Solid Fl -Rock C -Mud Dr -Wash I -Hand A	METHO Stem A light Au coring illing Drilling Luger	DD S Juger SS ger ST CR BS	AMPLIN - Split S - Shelb - Rock - Bag S	NG ME Spoon y Tube Core S ample	Samp Samp Sample	le * ple LL PL PI SF N6 N0	Al - Har - Liqu - Plas - Plas 7 - Star 0 - Star 0 - Star	BBREVIA ad Penetr id Limit stic Limit sticity Ind adard Pe adard Pe to 60%	omete ex netrati Drill R	on Tes on on od ER	st

		TES	ST BOF	RING	REC	ORD								
CLIEN	т:	Village West Alexandria					-		BO	RING NO	D.:	B-05	-18	
PROJE	ECT :	West Alexandria WWTP					_		SHE	ET	1	0	=	2
LOCAT	ION :	33 Desoto Drive					-		DAT	E STAR	RTED	: 03-2	6-18	
PROJE	CT NO. :	18050006CIN							DAT	E COM	PLETED	: 03-2	6-18	
BORIN	G ELEV	ATION : 879.7 Feet	RIG TYPE		: CME	45			DRI	LLER	:_0	os		
	NORT	HING : 641046.8441	CASING D	DIA.	: 3.25"				TEN	IPERAT	URE : 4	-0s		
	EAST	ING <u>: 1399240.1811</u>	CORE SIZ	Έ	: N/A				WE	ATHER	:_0	Cloudy		
	DEPT	H : 25.0 Feet	HAMMER		: Auto									
	BORI	NG METHOD: HSA	ENERGY I	RATIO	: 84.1									
GROU	NDWATE	R: $\mathbf{\Psi}$ Encountered at <u>13.5'</u> At cor	npletion <u>Dr</u>	<u>у</u>			1							
STRATUM ELEVATION	SAMPLE DEPTH		N	STRATUM DEPTH	SAMPLE NUMBER	SPT ber 6"	460	RECOVERY %)	MOISTURE CONTENT	FOTAL UNIT NEIGHT scf	JNCONF. COMP., ksf		ERBE .IMITS	ERG
0, 11		SOIL/MATERIAE DESCRIPTIO			0,2		~		20		20		ΓL	
					SS-1	2 3 4	10	100	22		8.0*			
	5	Medium Stiff to Stiff, Brown SANDY LEAN CLAY (CL), Moist			SS-2	2 3 3	8	56	17					
871.7_				8.0	SS-3	1 2 3	7	89			2.0*			
869.2_	10	Very Stiff, Brown SANDY LEAN CLAY (CL) Moist),	10.5	SS-4	6 7 8	21	89	11		7.5*			
					SS-5	1 2 2	6	56	16			NP	NP	NP
862.9	15	Loose, SILTY SAND with GRAVEL (SM), V	Vet	16.8	SS-6	2 2 2	6	44	1					
	20	Medium Dense, Gray WELL GRADED SAN with GRAVEL and SILTY CLAY (SW-SC) , Damp <i>Continued on next page</i>	JD		SS-7	5 6 7	18	67	7					
		2105 Schappelle Lane	BORIN	IG METH	DD S		IG ME	THOD		A	BBREVIA	TIONS	8	
	TL/ ERING ⁽²⁾	Cincinnati, Ohio 45240 Telephone: 513-722-8665 Fax: 513-834-6650 Email: ctlcin@ctleng.com	HSA-Holld SFA-Solid RC -Rock MD -Mud WD -Wasl HA -Hand	w Stem A I Flight Au Coring Drilling h Drilling d Auger	uger SS Iger ST CF BS	5 - Split S - Shelb R - Rock 5 - Bag S	Spoon y Tube Core S ample	Sample Sample Sample	e * ble LL PL PI SF N6	- Har - Liqu - Plas - Plas 7 - Stat 0 - Stat	nd Penetr uid Limit stic Limit sticity Ind ndard Pe ndard Pe	omete ex netrati netrati	r on Te on	st

			TES	ST BOR	ING	RECO	ORD								
CLIEN	Т		: Village West Alexandria					-		BOI	RING NC).:	B-05	5-18	
PROJE			: West Alexandria WWTP			1	1	1	1	SHE		2	0	F :	2
STRATUM ELEVATION	SAMPLE	DEPTH	SOIL/MATERIAL DESCRIPTIC)N	STRATUM DEPTH	SAMPLE NUMBER	SPT per 6"	N ₆₀	RECOVERY (%)	MOISTURE CONTENT	TOTAL UNIT WEIGHT pcf	UNCONF. COMP., ksf	ATT I	ERBE IMITS	RG PI
854.7_	25		Medium Dense, Gray WELL GRADED SA with GRAVEL and SILTY CLAY (SW-SC), Damp BOTTOM OF BORING	ND	25.0	SS-8	8 9 10	27	56	8					
	30	-													
	35	-													
	40	_													
	45	-													
			2105 Schappelle Lane Cincinnati, Ohio 45240 Telephone: 513-722-8665 Fax: 513-834-6650 Email: ctlcin@ctleng.com	BORIN HSA-Hollo SFA-Solid RC -Rock MD -Mud WD -Wasł HA -Hand	G METHO w Stem A Flight Au Coring Drilling Drilling Auger	DD S Auger SS Iger ST CR BS	AMPLIN - Split S - Shelb R - Rock - Bag S	NG ME Spoon y Tube Core S ample	Samp Samp Sample	le * ple LL e PL PI SF N6	Ali - Han - Liqu - Plas - Plas - Plas - Star - Star - Star - Star	BBREVIA Id Penetr Id Limit Stic Limit Sticity Ind Indard Pe Indard Pe I to 60%	omete ex netrati Drill R	s on Tea on od ER	st

			TES	ST BOP	RIN	G R	ECC	ORD								
CLIEN	Г	: Village Wes	st Alexandria								BO	RING NO	D.:	B-06	-18	
PROJE	СТ	: West Alexa	ndria WWTP								SHE	EET	1	0	=	2
LOCAT	ION	: 33 Desoto I	Drive								DAT	TE STAF	RTED	: 03-2	6-18	
PROJE	CT NO.	: 18050006C	IN								DAT	LE COM	PLETED	: 03-2	6-18	
BORIN	G ELE	VATION	: 881.9 Feet	RIG TYPE	E	:_	CME 4	5			DRI	LLER	:_[DS		
	NOF	RTHING	: 641047.8522	CASING [DIA.	:_	3.25"				TEN	IPERAT	URE : _4	l0s		
	EAS	TING	: 1399180.1896	CORE SIZ	ZE	:_	N/A				WE	ATHER	:_0	Cloudy		
	DEP	TH	: 30.0 Feet	HAMMER	R	:_	Auto									
	BOR	RING METHOD): HSA	ENERGY	RATI	0 :	84.1									
GROU	NDWAT	ER: 🗜 Enco	ountered at <u>5.0'</u> At cor	npletion <u>D</u>	ry											
STRATUM ELEVATION	SAMPLE DEPTH	c		N	TRATIM	DEPTH	SAMPLE JUMBER	SPT ber 6"	460	RECOVERY %)	AOISTURE CONTENT	OTAL UNIT VEIGHT ocf	JNCONF. COMP., ksf			RG
бш		3	UIL/MATERIAL DESCRIPTIO				0) 2	00	~	ШС	20	⊢> ¤	00	LL	PL	PI
						:	SS-1	3 3 3	8	100	16		3.0*			
_	 5	Loose, Brow	n CLAYEY SAND (SC) , Moist			:	SS-2	2 2 2	6	89	26			27	17	10
873.9_					8	.0	SS-3	2 3 4	10	100	12		3.5*			
	10	Very Stiff, G Moist (TILL)	ray SANDY LEAN CLAY (CL),			:	SS-4	4 5 7	17	100	16		7.0*			
868.9_					1:	3.0	SS-5	5 7 12	27	100	8		9.0*			
	15					:	SS-6	14 18 14	45	100	6					
		Dense, Brow	m WELL GRADED SAND with RAVEL (SW-SM), Moist			:	SS-7	13 15 17	45	100	5			NP	NP	NP
		2105 Sc	happelle Lane	BORI	NG ME	ETHOD) SA		IG ME	THOD		A	BBREVIA	TIONS	3	
	TL ERING ≌	Cincinna Telepho Fax: 51 Email: c	ati, Ohio 45240 ne: 513-722-8665 3-834-6650 xtlcin@ctleng.com	HSA-Hold SFA-Solid RC -Roc MD -Mud WD -Was HA -Han	ow Ste d Fligh k Cori d Drillir sh Dril nd Aug	em Aug ht Auge ing ng lling jer	ger SS er ST CR BS	- Split S - Shelby - Rock - Bag S	Spoon y Tube Core S ample	Sampl Samp Sample	e * ble LL PL PI SF N6	- Har - Liqu - Plas - Plas 2T - Stat - Stat	nd Penetr uid Limit stic Limit sticity Ind ndard Pe ndard Pe	omete lex netrati netrati	r on Te: on	st

ſ				TES	T BC	RI	NG I	REC	ORD								
	CLIEN	т	:	Village West Alexandria						_		BO	RING NO).:	B-06	6-18	
	PROJE	СТ	:	: West Alexandria WWTP								SHI	EET	2	0	F :	2
	STRATUM ELEVATION	SAMPLE		SOIL/MATERIAL DESCRIPTIO	N		STRATUM DEPTH	SAMPLE NUMBER	SPT per 6"	N ₆₀	RECOVERY (%)	MOISTURE	TOTAL UNIT WEIGHT pcf	UNCONF. COMP., ksf	ATT	ERBE LIMITS	RG PI
6/18	<u>LS</u> ∃∃	25_ 30_ 35_		SOIL/MATERIAL DESCRIPTION	J		<u>5</u> 円 _30.0	SS-8	9 12 13 10 14 17	35 43	型 ⁽ %) 56	4	TO WE WE			PL	Pl
XING/PIT RECORD 18050006CIN.GPJ CTL CORPORATE.GDT 5/1	5	45_		2105 Schappelle Lane Cincinnati, Ohio 45240 Telephone: 513-722-8665	BOI HSA-Ho SFA-So RC -Ro MD - M	RING bblow blid Fl ock C ud Dr	METHO Stem A ight Au oring illing	DD uger S ger S C B	SAMPLI S - Split T - Shelt R - Rock S - Bag S	NG ME Spoon by Tube Core S Sample	THOD Samp Sample Sample	le * ple LL e PI	Al - Har Liqu Plas - Plas	BBREVIA nd Penetr uid Limit stic Limit sticity Inc	TION	S er	
TEST BORIN	ENGINE	ERING	Ż	Fax: 513-834-6650 Email: ctlcin@ctleng.com	WD - W WD - W HA - Ha	ash E and A	ning Drilling uger	В	з-вад S	ample	;	SF Ne	Plas PT - Star 0 - Star 0 ormalized	ndard Pe ndard Pe <u>I to 60%</u>	netrat netrat <u>netrat</u> Drill_R	ion Te: ion <u>od E</u> R	st

		TES	ST BO	ORI	NG I	REC	ORD								
CLIEN	Г	: Village West Alexandria						_		BOI	RING NC	D.:	B-07	-18	
PROJE	СТ	:_West Alexandria WWTP						_		SHE	EET	1	0	=	2
LOCAT	ION	: 33 Desoto Drive						_		DA	TE STAR	RTED	: 03-2	7-18	
PROJE	CT NO.	: 18050006CIN								DA	LE COM	PLETED	: 03-2	7-18	
BORIN	G ELE	VATION : 884.4 Feet	RIG T	YPE		: CME 4	45			DRI	LLER	:_0	S		
	NOF	CTHING : 641049.1122	CASIN	IG DIA		: 3.25"				TEN	IPERAT	URE : 5	i0s		
	EAS	TING : 1399105.2002	CORE	SIZE		: N/A				WE	ATHER	:_0	Cloudy		
	DEP	TH : 25.0 Feet	HAMM	1ER		: Auto									
	BOR	ING METHOD: HSA	ENER	GY RA	TIO	: 84.1									
GROU	NDWAT	ER: Encountered at <u>None</u> At con	npletion	<u>Dry</u>											
STRATUM LEVATION	AMPLE DEPTH		N		STRATUM DEPTH	AMPLE JUMBER	SPT er 6"	160	RECOVERY %)	AOISTURE CONTENT	OTAL UNIT VEIGHT of	JNCONF. COMP., ksf	ATT	ERBE	ERG
ωш	00	SOIL/MATERIAL DESCRIPTION	N	V/////	00	Z	00	2	Щ	20	⊢> a	0	LL	PL	PI
						SS-1	3 3 4	10	100	24		3.0*			
	5	Medium Stiff to Stiff, Brown SANDY LEAN CLAY (CL), Wet				SS-2	2 2 3	7	0	14		5.0*			
						SS-3	2 3 5	11	67	14		2.5*			
873.9_	10				_10.5	SS-4	3 5 4	13	56	15		6.0*			
						SS-5	12 15 16	43	44	14					
867.7	15	Hard, Gray SANDY LEAN CLAY (CL) , Wet			16.8	SS-6	10 12 13	35	56	13		3.0*			
	20	Dense to Very Dense, Gray WELL GRADE SAND with SILTY CLAY and GRAVEL (SW-SC), Moist	D			SS-7	13 16 17	46	67	6					
;		2105 Schappelle Lane	BC	ORING	METHO	DD S	AMPLIN	NG ME	THOD		A	BBREVIA	TIONS	6	
	TL ERING ⁽²⁾	Cincinnati, Ohio 45240 Telephone: 513-722-8665 Fax: 513-834-6650 Email: ctlcin@ctleng.com	HSA-H SFA-S RC -F MD -N WD -V HA -H	Hollow Solid Fl Rock C Mud Dr Wash E Hand A	Stem A ight Au oring illing Drilling uger	uger SS ger ST CR BS	- Split S - Shelb - Rock - Bag S	Spoon y Tube Core S ample	Sampl Samp Sample	le * ple LL PL PI SF N6	- Har - Liqu - Plas - Plas - Plas - Stai - Stai	nd Penetr uid Limit stic Limit sticity Ind ndard Pe ndard Pe	omete ex netrati netrati	r on Te on	st

			TES	ST BOR	NG	RECO	ORD								
CLIEN	т		: Village West Alexandria					-		BOI	RING NC).:	B-07	′-1 8	
PROJE			: West Alexandria WWTP		1	1	1	1	1	SHE		2	0	F :	2
STRATUM ELEVATION	SAMPLE	DEPTH	SOIL/MATERIAL DESCRIPTIO	N	STRATUM DEPTH	SAMPLE NUMBER	SPT per 6"	N ₆₀	RECOVERY (%)	MOISTURE	TOTAL UNIT WEIGHT pcf	UNCONF. COMP., ksf	ATT I	ERBE IMITS	RG S
859.4_	25		Dense to Very Dense, Gray WELL GRADE SAND with SILTY CLAY and GRAVEL (SW-SC), Moist BOTTOM OF BORING	Ð	25.0	SS-8	12 18 20	53	56	5					
	30	-													
	35	-													
	40	-													
	45	-													
		⊥ 3≝	2105 Schappelle Lane Cincinnati, Ohio 45240 Telephone: 513-722-8665 Fax: 513-834-6650 Email: ctlcin@ctleng.com	BORING HSA-Hollow SFA-Solid F RC -Rock (MD -Mud D WD -Wash HA -Hand /	Stem A Stem A Clight Au Coring rilling Drilling Auger	L DD S Auger SS Iger ST CR BS	AMPLIN - Split S - Shelb - Rock - Bag S	NG ME Spoon y Tube Core s ample	Samp Samp Sample Sample	le * ple LL e PL SF N6	All - Han - Liqu - Plas - Plas - Plas - Star - Star - Star - Star	BBREVIA Id Penetr Id Limit Stic Limit Sticity Ind Indard Pe Indard Pe I to 60%	TION: omete ex netrati netrati	S on Tea on od ER	st

			TE	EST E	BORI	NG	REC	ORD								
CLIEN	т	: Village We	st Alexandria						_		BO	RING NO	D.:	B-08	8-18	
PROJE	ECT	: West Alexa	andria WWTP								SHI	EET	1	0	F	2
LOCAT	ΓΙΟΝ	: 33 Desoto	Drive						_		DA	TE STAF	RTED	: 03-2	27-18	
PROJE	ECT NO.	: 180500060	SIN						-		DA	ТЕ СОМ	PLETED	: 03-2	27-18	
BORIN	IG ELE	VATION	: 884.9 Feet	RIG	TYPE		: CME	45			DR	ILLER	: [DS		
	NOF	THING	: 641050.3722	CAS	ING DIA	۱.	: 3.25"				TEN	MPERAT	URE : 5	i0s		
	EAS	TING	: 1399030.2108		E SIZE		: N/A				WE	ATHER	: (Cloudv		
	DEP	TH	: 25.0 Feet	HAN	IMER		: Auto									
	BOR	ING METHO	D: HSA	ENE	RGY RA		: 84.1									
GROU	NDWAT	ER: 👤 Enc	ountered at <u>10.0'</u> Σ At o	completio	on <u>12.0'</u>		•									
TRATUM	AMPLE EPTH					TRATUM EPTH	AMPLE IUMBER	.PT er 6"	60	(ECOVERY %)	10ISTURE CONTENT	OTAL UNIT VEIGHT of	INCONF. OMP., ksf	ATT L		ERG
ωш	00	5	OIL/MATERIAL DESCRIPT	ION	V////	00	σz	0 0	2	R S	20	⊢ > ¤	50	LL	PL	PI
							SS-1	4 4 5	13	100	28		4.0*			
	5_	Stiff, Brown	SANDY LEAN CLAY (CL), N	∕loist			SS-2	3 5 3	11	67	25		3.0*			
877.9_						7.0	ST-3			100	27	124	0.7 @ 3.2%	26	16	10
	-10						SS-4	3 5 7	17	100	11		5.0*	22	14	8
<u> </u>		Stiff to Very (CL) , Wet (1	Stiff, Gray SANDY LEAN C I ILL)	LAY			SS-5	3 3 5	11	100	12		3.0*			
2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	15						SS-6	3 5 6	15	89	11		2.0*			
\$ 868.1_		Dense to Ve SAND with	ery Dense, Brown WELL GR GRAVEL (SW), Moist <u>Contin</u> ued on next page	ADED		16.8	SS-7	15 13 15	39	56	6					
		2105 Sc	happelle Lane	E	BORING	METH			NG ME	THOD		A	BBREVIA	TIONS	<u>S</u>	
	TL ERING ^z	Cincinna Telepho Fax: 51	HSA SFA RC MD WD	- Hollow - Solid F - Rock C - Mud Di - Wash I	Stem A light Au Coring rilling Drilling	uger St iger ST Cf Bt	S-Split S - Shelb R-Rock S-Bag S	spoon y Tube Core S Sample	Samp e Samj Sample e	ie ^ ole LL e PL PI SF	- Hai Liq - 2 Pla - 91a - 913 - 54a	nd Penetr uid Limit stic Limit sticity Ind indard Pe	lex netrati	on Te	st	
	Email: ctlcin@ctleng.com					uyer						ormalized	d to 60%	Drill R	od ER	

			TES	ST BORI	NG	RECO	ORD								
CLIEN	Т		: Village West Alexandria					-		BOI	RING NC	0.:	B-08	8-18	
PROJE			: West Alexandria WWTP		1		1	1	1	SHE		2	0	F	2
STRATUM ELEVATION	SAMPLE		SOIL/MATERIAL DESCRIPTIO	N	STRATUM DEPTH	SAMPLE NUMBER	SPT per 6"	N ₆₀	RECOVERY (%)	MOISTURE	TOTAL UNIT WEIGHT pcf	UNCONF. COMP., ksf		ERBE LIMITS	RG S
			Dense to Very Dense, Brown WELL GRAI SAND with GRAVEL (SW), Moist	DED		SS-8	15 18	53	67	6					
859.9_	25_	-	BOTTOM OF BORING		25.0		20								
	30_														
	35_	-													
	40_	-													
	45_	-													
			2105 Schappelle Lane Cincinnati, Ohio 45240 Telephone: 513-722-8665 Fax: 513-834-6650 Email: ctlcin@ctleng.com	BORING HSA-Hollow SFA-Solid F RC -Rock C MD -Mud D WD -Wash I HA -Hand A	METHO Stem A light Au Coring rilling Drilling Auger	DD S Auger SS Iger ST CR BS	AMPLIN - Split S - Shelb - Rock - Bag S	NG ME Spoon y Tube Core s ample	Samp Samp Sample Sample	le * ple LL e PL SF N6	All - Han - Liqu - Plas - Plas - Plas - Star - Star - Star - Star	BBREVIA Id Penetr Id Limit Stic Limit Sticity Ind Indard Pe Indard Pe I to 60%	TION: omete ex netrati netrati	S ion Tea ion od ER	st

		TE	ST B	ORI	NG	REC	ORD								
CLIEN	т	: Village West Alexandria						_		BOI	RING NC	D.:	B-09	-18	
PROJE	CT	: West Alexandria WWTP						_		SHE	EET	1	0	=	2
LOCAT	TION	: 33 Desoto Drive						-		DA	TE STAR	RTED	: 03-2	7-18	
PROJE	ECT NO.	: 18050006CIN						-		DA	LE COM	PLETED	: 03-2	7-18	
BORIN	IG ELE	VATION : 884.4 Feet	RIG 1	YPE		: CME	45			DRI	LLER	: [DS		
	NOF	THING : 641051.6322	CASI	NG DIA	۸.	: 3.25"					/IPERAT	URE : 5	50s		
	EAS	TING : 1398955.2214		E SIZE		: N/A				WE	ATHER	: (Cloudy		
	DFF	TH 25.0 Feet		MFR		· Auto									
	BOF			RGYR		· 84 1									
GROU	NDWAT	ER: Encountered at <u>None</u> At o	completio	n <u>Dry</u>						1					
z									٢		F	Ļ			-00
MOL	щ_				N	щК			/ER	IN T	Z ⊃⊢	, ksi		IMITS	RG S
EVAT	PTF				PTH	MPL	_ ⁵		CO	NTE	IGH	ÅP.			1
STI	SAI	SOIL/MATERIAL DESCRIPT	ION		STI	SAI	Per SP	2 ⁰⁰	RE (%)	80 N N	pg⊈d	NO NC	LL	PL	PI
	$+$						2								
	I IXI	Stiff, Brown SANDY LEAN CLAY (CL), N	loist			SS-1	3	10	100	16		2.0*			
	IΔ						4								
881.4					3.0										
	\square	Stiff Brown and Grav SANDY LEAN CL	^ V				2								
	ľ	(CL), Moist	~'			SS-2	3	11	100	17		3.0*			
878.9	5				55		5								
	1 🔟														
	I M					66.2	3	11	02	10		7.0*			
	-//					33-3	5		03	12		7.0			
		Stiff to Very Stiff, Brown SANDY LEAN	CLAY												
		(CL), Moist					2								
	I -VI					SS-4	5	17	100	10		9.0*			
	10_/						7								
873.9_					10.5										
							9								
		Hard, Brown SANDY LEAN CLAY (CL),	Moist			SS-5	11	36	56	10		9.0*			
071 /	IΑ				120		15								
0/1.4_					13.0										
					:		12								
5		Very Dense Brown SILTY CLAYEY SAI	ND			SS-6	15	60	67	12		3.0*			
5		(SC-SM),					20								
5															
867.7_					16.8										
		Dense, Gray WELL GRADED SAND wit	h				15								
	l -VI	SILTY CLAY and GRAVEL (SW-SC), We	et			SS-7	14	45	56	4					
	20_/				*		18								
		Continued on next page													
			В	ORING	METH	OD S		NG ME	THOD		A	BBREVIA	TIONS	3	
_			HSA-	Hollow	Stem A	AugerSS	-Split S	Spoon	Sampl		- Har	nd Penetr	romete	r	
			RC -	Solid F Rock (iight Au Corina	iger ST CF	- Sneib R-Rock	y Tube Core S	e Samp Sample	ne∣LL è∣PI	- Liqu - Plas	ua Limit stic Limit			
		Fair 542 004 0050	MD -	Mud D	rilling	BS	-Bag S	ample)	PI	- Plas	sticity Ind	lex		
	EKING≧	Fax: 513-834-6650	WD -	Wash	Drilling					SF	PT - Star	ndard Pe	netrati	on Te	st
2		Email: ctlcin@ctleng.com	HA -	riang A	vuger						ormalized	to 60%	Drill R	on od ER	

			TES	st Bof	RING	REC	ORD								
CLIEN	Т		: Village West Alexandria					-		BOI	RING NC).:	B-09	9-18	
PROJE			: West Alexandria WWTP			1			1	SHE	EET	2	0	F	2
STRATUM ELEVATION	SAMPLE	DEPIH	SOIL/MATERIAL DESCRIPTIC	DN	STRATUM DEPTH	SAMPLE NUMBER	SPT per 6"	N ₆₀	RECOVERY (%)	MOISTURE	TOTAL UNIT WEIGHT pcf	UNCONF. COMP., ksf		ERBE LIMITS	RG PI
859.4	25		Dense, Gray WELL GRADED SAND with SILTY CLAY and GRAVEL (SW-SC), Wet		25.0	SS-8	15 16 17	46	56	4					
000.4		-	BOTTOM OF BORING	••	<u>~ ~</u> _ C. U										
	30	-													
	35	-													
	40	-													
	45	-													
			2105 Schappelle Lane Cincinnati, Ohio 45240 Telephone: 513-722-8665 Fax: 513-834-6650 Email: ctlcin@ctleng.com	BORIN HSA-Hollo SFA-Solio RC -Rock MD -Mud WD -Was HA -Hano	NG METH ow Stem / d Flight Ar Coring Drilling h Drilling d Auger	Auger SS Jger ST CF BS	SAMPLIN S - Split S - Shelb R - Rock S - Bag S	NG ME Spoon y Tub Core s ample	Samp Samp Sample	le * ple LL e PL SF NG	Al - Har - Liqu - Plas - Plas - Plas - Star - Star - Star - Star	BBREVIA Id Penetr Id Limit Stic Limit Sticity Ind Indard Pe Indard Pe I to 60%	omete ex netrati Drill R	S ion Tea ion od ER	st

			•	TEST	BORI	NG	REC	ORD								
CLIEN	т	: Village We	st Alexandria						_		BO	RING NC	D.:	B-10	-18	
PROJE	СТ	: West Alexa	andria WWTP						_		SHI	EET	1	OF	:	1
LOCAT	TION	: 33 Desoto	Drive						_		DA	TE STAR	RTED	: 03-2	6-18	
PROJE	ECT NO.	: 180500060	CIN								DA	TE COM	PLETED	: 03-2	6-18	
BORIN	IG ELE	VATION	: 879.7 Feet	R	IG TYPE		: CME	45			DR	LLER	: 0	DS		
	NOF	RTHING	: 641111.8350	C	ASING DIA	۱.	: 3.25"					IPERAT	URE:4	0s		
	EAS	TING	: 1399241.2732	c	ORE SIZE		: N/A				WE	ATHER	: 0	Cloudy		
	DEF	тн	: 10.0 Feet	н	AMMER		: Auto									
	BOF	RING METHO	D: HSA	E	NERGY RA		: 84.1									
GROU	NDWAT	ER: Enc	ountered at <u>None</u>	At compl	letion <u>Dry</u>											
LEVATION	AMPLE EPTH					FRATUM EPTH	AMPLE UMBER	oT sr 6"	80	ECOVERY 6)	OISTURE	DTAL UNIT EIGHT 양	NCONF. OMP., ksf	ATT	ERBE	ERG
ы	δā	S	OIL/MATERIAL DESCR	RIPTION		50	δź	Lig a	z	28	Σŭ	₽≥₫	Ξŭ	LL	PL	PI
							SS-1	2 3 4	10	100	27		3.5*			
	5	Stiff, SAND '	Y LEAN CLAY (CL), Mois	st			SS-2	3 3 4 2	10	67	14		5.5*			
							SS-3	46	14	100	14		3.5*			
869.7_	10	воттом о	FBORING			10.0	SS-4	3 4 5	13	56	11		3.0*			
06CIN.GPJ CTL CORPORATE.GDT 5/16/18																
80500(
02 		0405.0			BORING	METH	ן סכ	SAMPLI	NG ME	THOD		A	BBREVIA		\$	
	TL ering ≌	Cincinna Telepho Fax: 51 Email:	H S R M W H	SA-Hollow FA-Solid F C -Rock C ID -Mud D /D -Wash I A -Hand A	Stem A light Au Coring rilling Drilling Nuger	Auger St Iger S Cl Bt	S - Split { Γ - Shelb R - Rock S - Bag S	Spoon y Tube Core S Sample	Samp e Samp Sample	le * ple LL PL PI SF Ne No	- Har - Liqu - Plas - Plas - Plas - Star - Star - Star - Star	nd Penetr uid Limit stic Limit sticity Ind ndard Pe ndard Pe I to 60%	omete lex netration Drill Ro	r on Te on od ER	st	

			TE	ST B	ORI	NG	REC	ORD								
CLIEN	Г	: Village Wes	st Alexandria						_		BO	RING NO	D.:	B-11	-18	
PROJE	CT	: West Alexa	ndria WWTP						_		SHI	EET	1	0	F	2
LOCAT	ION	: 33 Desoto I	Drive						_		DA	TE STAF	RTED	: 03-2	6-18	
PROJE	ECT NO.	: 18050006C	IN								DA	TE COM	PLETED	: 03-2	6-18	
BORIN	G ELE	VATION	: 880.8 Feet	RIG T	YPE		: CME	45			DR	LLER	:_0	DS		
	NOF	RTHING	: 641112.8430	CASIN	NG DIA	۱.	: 3.25"				TEN	IPERAT	URE : 4	l0s		
	EAS	TING	: 1399181.2816	CORE	SIZE		: N/A				WE	ATHER	: 0	Cloudy		
	DEP	TH	: 25.0 Feet	HAMN	/IER		: Auto									
	BOF	NING METHOE): HSA	ENER	GY RA	TIO	: 84.1									
GROU	NDWAT	ER: Enco	ountered at <u>None</u> At co	mpletior	n <u>Dry</u>	1	1	-	1					1		
RATUM EVATION	MPLE EPTH					-RATUM EPTH	MPLE JMBER	JT r 6"	0	ECOVERY	DISTURE	DTAL UNIT EIGHT f	VCONF. DMP., ksf	ATT	ERBE	ERG
ELST	SA DE	S	OIL/MATERIAL DESCRIPTIC	ON		ST	S^ NC	Pe Pe	z	R%	Σŭ	Pi≱g	Ξŭ	LL	PL	PI
877.8	-X	Stiff, Brown	SANDY LEAN CLAY (CL), Mo	vist		3.0	SS-1	3 3 4	10	100	21		5.0*			
	5						SS-2	2 2 3	7	100	13		5.5*			
		Medium Stiff CLAY (CL-M	i to Stiff, Brown SANDY SILT Y L), Moist	ſ			SS-3	3 4 5	13	67	12		3.5*			
870.3_	10					10.5	SS-4	4 5 6	15	100	13		6.5*	21	14	7
							SS-5	20 20 13	46	67	6					
. CORPORATE.GDT 5/16/18	15	Dense, Brow SILTY CLAY	/n WELL GRADED SAND witi and GRAVEL (SW-SC), Mois	h st			SS-6	3 15 11	36	56	5					
18050006CIN.GPJ CT	20		Continued on next page				SS-7	11 13 15	39	67	5					
CORE		2105 Sc	happelle Lane	BC		METHO				THOD	<u>ا</u> ما		BBREVIA	TIONS	6 r	
BORING/PIT REC	TL ERING ^Z	Cincinna Telephor Fax: 513	ati, Ohio 45240 ne: 513-722-8665 3-834-6650	SFA-S RC -I MD -I WD -V	Solid F Rock C Mud Dr Wash [light Au coring rilling Drilling	iger ST CF BS	- Shelb R - Rock S - Bag S	y Tube Core S ample	e Samp Sample	ple LL PL PI SF	- Har - Liqu - Pla: - Pla: - Pla: - Sta	uid Limit stic Limit sticity Ind ndard Pe	lex netrati	on Te	st
TES	Email: ctlcin@ctleng.com					uyer						ormalized	d to 60%	Drill R	on od ER	

			TES	ST BORI	NGI	RECO	ORD								
CLIEN	IT		: Village West Alexandria							BO	RING NC	0.:	B-1 1	-18	
PROJI	ECT		: West Alexandria WWTP							SHE	EET	2	0	F 2	2
STRATUM ELEVATION	SAMPLE	DEPTH	SOIL/MATERIAL DESCRIPTIC	N	STRATUM DEPTH	SAMPLE NUMBER	SPT per 6"	N ₆₀	RECOVERY (%)	MOISTURE CONTENT	TOTAL UNIT WEIGHT pcf	UNCONF. COMP., ksf	ATT I	ERBE IMITS	RG PI
855.8 ₋	_ 25		Dense, Brown WELL GRADED SAND with SILTY CLAY and GRAVEL (SW-SC), Mois BOTTOM OF BORING	n t	_25.0	SS-8	4 12 13	35	44	5					
	30														
	35														
	40														
	45	-													
		⊥ G≦	2105 Schappelle Lane Cincinnati, Ohio 45240 Telephone: 513-722-8665 Fax: 513-834-6650 Email: ctlcin@ctleng.com	BORING HSA-Hollow SFA-Solid FI RC -Rock C MD -Mud Dr WD -Wash E HA -Hand A	METHO Stem A ight Au oring illing Drilling uger	DD S uger SS ger ST CR BS	- Split S - Shelby - Rock - - Bag S	i G ME spoon y Tube Core s ample	Samp Samp Sample Sample	le * ple LL e PL PI SF N6 Nc	Al - Har - Liqu - Plas - Plas 2T - Stal 0 - Stal prmalized	BBREVIA ad Penetr uid Limit stic Limit sticity Ind ndard Pe ndard Pe I to 60%	omete ex netrati Drill R	s on Tes on od ER	st

	TES	T BORI	NG I	RECO	ORD								
CLIENT	: Village West Alexandria					_		BOI	RING NC	D.:	B-12	2-18	
PROJECT	: West Alexandria WWTP					-		SHE	EET	1	0	F	2
LOCATION	: 33 Desoto Drive					-		DA	TE STAR	RTED	:_03-2	26-18	
PROJECT NO	: 18050006CIN							DA		PLETED	: 03-2	6-18	
BORING ELE	VATION : 882.3 Feet	RIG TYPE		: CME 4	15			DRI	LLER	:_0)S		
NO	RTHING <u>: 641114.1030</u>	CASING DIA		: 3.25"				TEN	/IPERAT	URE : 4	0s		
EAS	TING <u>1399106.2922</u>	CORE SIZE		: N/A				WE	ATHER	:_0	Cloudy		
DEI	25.0 Feet	HAMMER		: Auto									
BOI	RING METHOD: HSA	ENERGY RA	TIO	: 84.1									
GROUNDWAT	ER: Encountered at <u>None</u> At con	npletion <u>Dry</u>	1		1								
STRATUM ELEVATION SAMPLE DEPTH	SOIL/MATERIAL DESCRIPTIO	N	STRATUM DEPTH	SAMPLE NUMBER	SPT per 6"	N ₆₀	RECOVERY (%)	MOISTURE CONTENT	TOTAL UNIT WEIGHT pcf	UNCONF. COMP., ksf		ERBE IMITS	RG PI
						-							
				SS-1	2 3 3	8	100	28		4.5*			
5_	Medium Stiff, Brown SANDY LEAN CLAY (CL), Moist			SS-2	1 2 3	7	100	20		1.5*			
				SS-3	2 2 3	7	100	21					
871.8			_10.5	SS-4	2 1 3	6	89	16					
869.3	Stiff, Brown SANDY LEAN CLAY (CL), Mois	st	_13.0	SS-5	3 5 5	14	100	11		6.5*			
15_	Very Loose, SILTY SAND with GRAVEL (S Wet	M),	16.9	SS-6	3 2 1	4	67	14			NP	NP	NP
20	Medium Dense, Brown WELL GRADED SA with SILTY CLAY and GRAVEL (SW-SC), Moist	ND		SS-7	4 4 6	14	67	8					
	2105 Schappelle Lane	BORING	METHO	DD S		IG ME	THOD		A	BBREVIA	TIONS	6	•
	Cincinnati, Ohio 45240 Telephone: 513-722-8665 Fax: 513-834-6650 Email: ctlcin@ctleng.com	HSA-Hollow SFA-Solid F RC -Rock C MD -Mud Dr WD -Wash I HA -Hand A	Stem A light Au coring illing Drilling Luger	uger SS Iger ST CR BS	- Split S - Shelby - Rock - Bag S	Spoon y Tube Core S ample	Sampl e Samp Sample e	le * ple LL PL PI SF N6	Har - Har - Liqu - Liqu - Plas - Plas - Stai - Stai	nd Penetr uid Limit stic Limit sticity Ind ndard Pe ndard Pe	omete lex netrati netrati	r on Te on	st

			TES	ST BORI	NG	RECO	ORD								
CLIEN	Т		: Village West Alexandria					-		BOI	RING NC).:	B-12	2-18	
PROJE			: West Alexandria WWTP				1	1	1	SHE		2	0	F	2
STRATUM ELEVATION	SAMPLE	DEPIH	SOIL/MATERIAL DESCRIPTIC)N	STRATUM DEPTH	SAMPLE NUMBER	SPT per 6"	N ₆₀	RECOVERY (%)	MOISTURE	TOTAL UNIT WEIGHT pcf	UNCONF. COMP., ksf	ATT I	ERBE LIMITS	RG PI
857.3_	25		Medium Dense, Brown WELL GRADED SA with SILTY CLAY and GRAVEL (SW-SC), Moist BOTTOM OF BORING	AND	_25.0	SS-8	5 6 7	18	56	6					
	30	-													
	35	-													
	40	-													
	45	-													
			2105 Schappelle Lane Cincinnati, Ohio 45240 Telephone: 513-722-8665 Fax: 513-834-6650 Email: ctlcin@ctleng.com	BORING HSA-Hollow SFA-Solid F RC -Rock C MD -Mud Dr WD -Wash I HA -Hand A	METHO Stem A light Au coring illing Drilling Luger	DD S Auger SS Iger ST CR BS	AMPLIN - Split S - Shelb - Rock - Bag S	NG ME Spoon y Tube Core s ample	Samp Samp Sample Sample	le * ple LL e PL SF N6	All - Han - Liqu - Plas - Plas - Plas - Star - Star - Star - Star	BBREVIA Id Penetr Iid Limit Stic Limit Sticity Ind Indard Pe Indard Pe I to 60%	TION: omete ex netrati Drill R	S ion Tea ion od ER	st

CME 45 3.25" N/A Auto 84.1		BORING SHEET DATE ST DATE CO DRILLER TEMPER WEATHE	NO.:1	B-13- OF : 03-23 : 03-23 OS : 03-23 OS : 03-23 OS : 03-23 : 03-23 : 03-23 : 03-23 : 03-23 : 03-23 : 03-23 : 03-23 : 05 : 05 : 05 : 05 : 05 : 05 : 05 : 05	<u>2</u> -18 -18	
CME 45 3.25" N/A Auto 84.1		SHEET DATE ST DATE CO DRILLER TEMPER WEATHE	1 TARTED OMPLETED R :E RATURE :_4 ER :_C	OF : <u>03-23</u> : <u>03-23</u> OS OS Clear	2 -18 -18	
CME 45 3.25" N/A Auto 84.1		DATE ST DATE CO DRILLER TEMPER WEATHE	TARTED OMPLETED R : <u>E</u> RATURE : <u>4</u> ER : <u>C</u>	: 03-23 : 03-23 DS 0s Clear	-18 -18	
CME 45 3.25" N/A Auto 84.1		DATE CO DRILLER TEMPER WEATHE	OMPLETED R : _[RATURE : _4 ER : _(: 03-23 DS 0s Clear	-18	
CME 45 3.25" N/A Auto 84.1		DRILLER TEMPER WEATHE	R : <u>[</u> RATURE : <u>4</u> ER : <u>(</u>	OS IOs Clear		
3.25" N/A Auto 84.1		TEMPER	RATURE : _4 ER : _(l0s Clear		
N/A Auto 84.1		WEATHE	ER : <u>(</u>	Clear		
Auto 84.1						
84.1						
ш к						
<i>.</i>						
SAMPLI NUMBE SPT per 6"	N ₆₀ RECOVERY (%)	MOISTURE CONTENT TOTAL UNIT WEIGHT	pcf UNCONF. COMP., ksf		RBERG MITS PL PI	
SS-1 5 6	15 100	25	6.5*			
SS-2 4 5	13 100	18	6.0*			
SS-3 7 8	21 100	12	9.0*			
6 SS-4 9 12	29 100	12	5.0*			
SS-5 2 3	7 100	14	4.0*	21	14 7	
SS-6 2 1	4 56	16	2.5*			
SS-7 10 22	53 100	7				
D SAMPLIN	IG METHOD		ABBREVIA	TIONS		
ugerISS - Split S ger ST - Shelby CR - Rock (BS - Bag S	ippoon Sample * - Hand Penetrometer y Tube Sample LL - Liquid Limit Core Sample PL - Plastic Limit ample PI - Plasticity Index SPT - Standard Penetration Test Nac Standard Penetration					
	Import Import SS-1 3 SS-1 5 6 4 SS-2 4 SS-3 7 SS-3 4 SS-4 9 12 2 SS-5 2 SS-5 2 SS-6 2 SS-7 10 SS-7 10 Independence 10 SS-7 10 </td <td>Image Image <thimage< th=""> <thimage< th=""> <thi< td=""><td>\underline{W} \underline{L} \underline{v} \underline{v} \underline{W} \underline{W}</td><td>$\overline{WO}$$\overline{L}$ $\overline{O}$$\overline{C}$ $\overline{C}$$\overline{C}$ $\overline{C}$$\overline{O}$ $\overline{V}$$\overline{O}$ </td><td>with 0 1 1 0 2 0 1 1 1 1 SS-1 3 15 100 25 6.5* 6.5* 1 1 SS-2 4 13 100 18 6.0* 1</td></thi<></thimage<></thimage<></td>	Image Image <thimage< th=""> <thimage< th=""> <thi< td=""><td>\underline{W} \underline{L} \underline{v} \underline{v} \underline{W} \underline{W}</td><td>$\overline{WO}$$\overline{L}$ $\overline{O}$$\overline{C}$ $\overline{C}$$\overline{C}$ $\overline{C}$$\overline{O}$ $\overline{V}$$\overline{O}$ </td><td>with 0 1 1 0 2 0 1 1 1 1 SS-1 3 15 100 25 6.5* 6.5* 1 1 SS-2 4 13 100 18 6.0* 1</td></thi<></thimage<></thimage<>	\underline{W} \underline{L} \underline{v} \underline{v} \underline{W}	\overline{WO} \overline{L} \overline{O} \overline{C} \overline{C} \overline{C} \overline{C} \overline{O} \overline{V} \overline{O} 	with 0 1 1 0 2 0 1 1 1 1 SS-1 3 15 100 25 6.5* 6.5* 1 1 SS-2 4 13 100 18 6.0* 1	

			TES	st Bof	RING	REC	ORD								
CLIEN.	т		: Village West Alexandria					-		BOI	RING NC).:	B-13	8-18	
PROJE			: West Alexandria WWTP			1	-			SHE	EET	2	0	F	2
STRATUM ELEVATION	SAMPLE		SOIL/MATERIAL DESCRIPTIC	DN 27	STRATUM DEPTH	SAMPLE NUMBER	SPT per 6"	N ₆₀	RECOVERY (%)	MOISTURE CONTENT	TOTAL UNIT WEIGHT pcf	UNCONF. COMP., ksf		ERBE LIMITS	RG PI
857.9_	25_		Very Dense, Brown SILTY CLAYEY SANE with GRAVEL (SC-SM),	þ	_25.0	SS-8	12 22 28	70	100	4					
		-	BOTTOM OF BORING												
	30_	_													
	35_	-													
	40_	-													
	45_	-													
	ERING		2105 Schappelle Lane Cincinnati, Ohio 45240 Telephone: 513-722-8665 Fax: 513-834-6650 Email: ctlcin@ctleng.com	BORII HSA-Holk SFA-Solic RC -Roc MD -Mud WD -Was HA -Han	NG METH by Stem J d Flight Ai k Coring Drilling h Drilling d Auger	OD S Auger SS Jger ST CF BS	SAMPLII S - Split S - Shelb R - Rock S - Bag S	NG ME Spoon y Tube Core S Sample	Samp Samp Sample	le * ple LL e PL PI SF N6	Al - Har - Liqu - Plas - Plas 2T - Star 50 - Star 50 - Star	BBREVIA ad Penetr id Limit stic Limit sticity Ind indard Pe indard Pe to 60%	omete ex netrati Drill R	s ion Tea ion od ER	st

			TES	ST B	ORI	NG	REC	ORD)							
CLIEN	Т	: Village Wes	st Alexandria						_		BOI	RING NO	D.:	B-14	-18	
PROJE	СТ	: West Alexa	ndria WWTP						_		SHE	EET	1	0	F:	2
LOCAT	ION	: 33 Desoto I	Drive						_		DA	TE STAF	RTED	: 03-2	23-18	
PROJE	ECT NO.	: 18050006C	IN								DA	TE COM	PLETED	: 03-2	23-18	
BORIN	G ELE	VATION	: 882.4 Feet	RIG T	YPE		: CME	45			DRI	LLER	:_[DS		
	NO	RTHING	: 641116.6230	CASI	NG DIA	۱.	: 3.25'				TEN	IPERAT	URE : 4	l0s		
	EAS	STING	: 1398956.3134	CORE	E SIZE		: N/A				WE	ATHER	:_0	Clear		
	DEF	РΤΗ	: 25.0 Feet	НАМ	/IER		: Auto									
	BOF	RING METHOD): HSA	ENER	GY RA	TIO	: 84.1									
GROU	NDWAT	ER: Enco	ountered at <u>None</u> At co	mpletio	n <u>Dry</u>	1	1							1		
-RATUM EVATION	MPLE EPTH					-RATUM EPTH	AMPLE JMBER	от r 6"	00	ECOVERY	OISTURE ONTENT	DTAL UNIT EIGHT f	VCONF. DMP., ksf	ATT		ERG
EST	2 2 2	S	OIL/MATERIAL DESCRIPTIC	ON		2 2 2 2	l 2 ĭ	Per Per	z	88	žŭ	F≥g	Ξŭ	LL	PL	PI
879.4_		Stiff, Brown I Organics	LEAN CLAY (CL), Moist, with			3.0	SS-1	3 3 6	13	100	23		5.0*			
	5_						SS-2	3 4 3	10	100	26					
		Stiff to Very (CL), Wet (T	Stiff, Brown SANDY LEAN CL ILL)	_AY			SS-3	3 6 7	18	100	12		4.5*			
871.9_	10					_10.5	SS-4	4 4 7	15	100	13		4.5*			
869.4_		Hard, Gray S	SANDY LEAN CLAY (CL), Dar	mp		13.0	SS-5	7 10 12	31	100	10		6.5*			
865.6	15	Medium Den with SILTY (Moist	ise, Brown WELL GRADED S CLAY and GRAVEL (SW-SC),	AND		_16.8	SS-6	6 9 11	28	100	8					
	20	Dense to Ve SAND with S (SW-SC), Mo	ry Dense, Gray WELL GRAD SILTY CLAY and GRAVEL bist Continued on next page	ED			SS-7	10 16 19	49	100	5					
		2105 Sc	happelle Lane	B	ORING	METH	DD	SAMPLI	NG ME	THOD		A	BBREVIA	TIONS	3	
Cincinnati, Ohio 45240HSA-HollCincinnati, Ohio 45240SFA-SoliCincinnati, Ohio 45240RC -RocTelephone: 513-722-8665RC -RocMD -MucWD -WasEmail: ctlcin@ctleng.comHA -Han							Auger S Iger S C B	S - Split S T - Shelb R - Rock S - Bag S	Spoon y Tube Core S Sample	Samp e Sam Sample e	le * ple LL e PL PI SF	- Har - Liqu - Plas - Plas - Plas - Sta - Sta	nd Penetr uid Limit stic Limit sticity Ind ndard Pe ndard Pe	omete lex netrati netrati	r ion Te	st

			TES	ST BOR	ING	RECO	ORD								
CLIEN	Т		: Village West Alexandria					-		BOI	RING NC	D.:	B-14	1-18	
PROJE			: West Alexandria WWTP				1	1		SHE	EET	2	0	F	2
STRATUM ELEVATION	SAMPLE	UEPIH	SOIL/MATERIAL DESCRIPTIC	DN	STRATUM DEPTH	SAMPLE NUMBER	SPT per 6"	N ₆₀	RECOVERY (%)	MOISTURE	TOTAL UNIT WEIGHT pcf	UNCONF. COMP., ksf			RG PI
857.4_	25	-	Dense to Very Dense, Gray WELL GRAD SAND with SILTY CLAY and GRAVEL (SW-SC), Moist BOTTOM OF BORING	ED	25.0	SS-8	12 20 23	60	100	7					
	30	-													
2	35 40	-													
	45	-													
			2105 Schappelle Lane Cincinnati, Ohio 45240 Telephone: 513-722-8665 Fax: 513-834-6650 Email: ctlcin@ctleng.com	BORING HSA-Hollov SFA-Solid RC -Rock MD -Mud E WD -Wash HA -Hand	S METH v Stem A Flight Au Coring Drilling Drilling Auger	DD S Auger SS Iger ST CR BS	AMPLIN - Split S - Shelb - Rock - Bag S	NG ME Spoon y Tube Core S ample	Samp Samp Sample	le * ple LL e PL PI SF N6	Al - Har - Liqu - Plas - Plas 2T - Stai 0 - Stai prmalized	BBREVIA ad Penetr uid Limit stic Limit sticity Ind ndard Pe ndard Pe I to 60%	omete ex netrat Drill R	S er ion Te ion od ER	st

			TES	ST B	ORI	NG	REC	ORD)							
CLIEN	Г	: Village West	Alexandria						_		BO	RING NO	D.:	B-15	-18	
PROJE	CT	: West Alexan	dria WWTP						_		SHI	EET	1	0	=	1
LOCAT	ION	: 33 Desoto D	rive						_		DA	TE STAF	RTED	: 03-2	2-18	
PROJE	CT NO.	: 18050006CII	N								DA	TE COM	PLETED	: 03-2	2-18	
BORIN	G ELE	VATION :	880.4 Feet	RIG T	YPE		: CME	45				ILLER	:_[DS		
	NOF	RTHING :	641117.8830	CASIN	IG DIA	۱.	: 3.25	•				MPERAT	URE : 3	80s		
	EAS	TING :	1398881.3240	CORE	SIZE		: N/A				WE	ATHER	:_0	Clear		
	DEP	РТН <u>:</u>	20.0 Feet	HAMM	1ER		: Auto				-					
	BOF	RING METHOD:	HSA	ENER	GY RA	TIO	: 84.1									
GROU	NDWATI	ER: Encou	Intered at <u>None</u> At cor	npletior	<u>Dry</u>	-	1			1						
RATUM EVATION	(MPLE EPTH					RATUM EPTH	MPLE JMBER	T 6"	0	ECOVERY	DISTURE	DTAL UNIT EIGHT f	JCONF. JMP., ksf	ATT	ERBE	ERG
ST	SADE	SO	IL/MATERIAL DESCRIPTIO	N	177777	DE ST	S^ N	Pe Pe	z	88	ΣŬ	P≥g	Ξŭ	LL	PL	ΡI
		Loose, Brown	CLAYEY SAND (SC), Moist				SS-1	3 3 4	10	100	24		6.5*			
874.9_	5					5.5	SS-2	23	7	100	26		2.0*	41	17	24
		Stiff to Very S (CL), Moist (T	AY			SS-3	3 4 4 6	11	100	12		5.5*				
869.9_	10					10.5	SS-4	8 10	25	100	11		7.0*			
	-/	Medium Dens	e to Dense, Brown WELL				SS-5	8 18	36	100	9					
	15	GRADED SAN GRAVEL (SW	-SC), Moist				SS-6	5 7 9	22	100	7					
863.7_		Dense, Gray SILTY CLAY a	NELL GRADED SAND with and GRAVEL (SW-SC), Moist	<u>t</u>		_16.8 _20.0	SS-7	13 17 16	46	100	6					
nene		BOTTOM OF	BORING													
		2105 000		BC	ORING	METHO	DD	SAMPLI	NG ME	THOD		A	BBREVIA		<u> </u>	
	Cincinnati, Ohio 45240 Telephone: 513-722-8665 Fax: 513-834-6650 Email: ctlcin@ctleng.com					HSA-Hollow Stem Auger SFA-Solid Flight Auger RC - Rock Coring MD - Mud Drilling WD - Wash Drilling					Spoon Sample * - Hand Penetrometer y Tube Sample LL - Liquid Limit Core Sample PL - Plastic Limit Sample PI - Plasticity Index SPT - Standard Penetration Test					
			icin@cueng.com								No	ormalized	d to 60%	Drill Ro	od ER	

			-	TEST	BORI	NG	REC	ORD)							
CLIEN	т	: Village	West Alexandria						_		BO	RING NO	D.:	B-16	-18	
PROJE	СТ	: West A	exandria WWTP						_		SHI	EET	1	OF	=	1
LOCAT	TION	: 33 Desc	oto Drive								DA	TE STAR	RTED	: 03-2	6-18	
PROJE	ECT NC). : 180500	D6CIN								DA	TE COM	PLETED	: 03-2	6-18	
BORIN	IG EL	EVATION	: 879.6 Feet	RI	G TYPE		: CME	45			DR	LLER	: [bs		
	NC	RTHING	: 641155.4978	CA	ASING DIA	۸.	: 3.25					IPERAT	URE : 4	0s		
	EA	STING	: 1399188.4995		ORE SIZE		: N/A				WE	ATHER	: 0	Cloudy		
	DE	PTH	: 10.0 Feet	 H4	AMMER		: Auto				-					
	BC	RING METH	HOD: HSA	EN	NERGY RA		: 84.1				-					
GROU	NDWA	TER: E	Encountered at <u>None</u>	At comple	etion <u>Dry</u>											
-RATUM EVATION	AMPLE EPTH					-RATUM EPTH	AMPLE JMBER	oT r 6"	00	ECOVERY	OISTURE ONTENT	DTAL UNIT EIGHT f	VCONF. DMP., ksf	ATT	ERBE .IMITS	RG
ы	2 2 2		SOIL/MATERIAL DESCR	IPTION	V/////	5 2 2	δĨ	P S F	z	88	žŭ	F≥g	Ξŭ		PL	ΡI
876.6_		Medium (CL), Mo	Stiff, Brown LEAN CLAY wit ist	th SAND		3.0	SS-1	2 2 3	7	100	23		4.5*			
	5_						SS-2	3 3 3	8	100	16		3.0*			
		Medium CLAY (C	Stiff to Stiff, Brown SANDY I L), Moist	LEAN			SS-3	2 2 3	7	56	14		2.0*			
869.6_	 10	BOTTON	I OF BORING			10.0	SS-4	2 3 4	10	67	15		3.5*			
6CIN.GPJ CTL CORPORATE.GDT 5/16/18																
XD 1805000	20_				BORING	METH							BBRE\/IA			
	2105 Schappelle Lane Cincinnati, Ohio 45240 Telephone: 513-722-8665 Fax: 513-834-6650 Email: ctlcin@ctleng.com				SA-Hollow A-Solid F C -Rock C D -Mud Di D -Wash I A -Hand A	Stem A light Au Coring rilling Drilling Auger	Auger S Iger S C B	S - Split S T - Shelb R - Rock S - Bag S	Spoon by Tube Core S Sample	Samp Sample Sample	le * ple LL e PL PI SF Ng	- Har - Liqu - Plas - Plas 2T - Stai 50 - Stai	nd Penetr uid Limit stic Limit sticity Ind ndard Pe ndard Pe d to 60%	lex netrati netrati	r on Te: on od ER	st

				TES	T BOI	RIN	NG I	REC	ORD								
CLIENT	г	: Village We	est Alexandria							_		BO	RING NO	D.:	B-17	-18	
PROJE	СТ	: West Alex	andria WWTP							_		SHI	EET	1	0	=	1
LOCAT	ION	: 33 Desoto	Drive							_		DA	TE STAF	RTED	:_03-2	8-18	
PROJE	CT NO	. : 18050006	CIN									DA	LE COM	PLETED	: 03-2	8-18	
BORIN	G ELI	EVATION	: 862.8 Feet	F	RIG TYPI	E		: CME	45			DR	LLER	: <u> </u>)S		
	NO	RTHING	: 641228.0899		CASING	DIA.		: 3.25"					/ PERAT	URE : 4	0s		
	EA	STING	: 1399276.4504	(CORE SI	ZE		: N/A				WE	ATHER	:_0	Cloudy		
	DE	PTH	: 10.0 Feet	ŀ	HAMMER	2		: Auto									
	BO	RING METHO	D: HSA	E	ENERGY	RA1	τιο	: 84.1									
GROU	NDWA	TER: End	countered at <u>None</u>	At comp	oletion <u>D</u>	ry				1	1						
-RATUM EVATION	AMPLE EPTH						-RATUM EPTH	AMPLE JMBER	оТ ir 6"	00	ECOVERY	OISTURE ONTENT	DTAL UNIT EIGHT f	VCONF. DMP., ksf	ATT	ERBE	ERG
БIJ	2S/ DE	5	OIL/MATERIAL DESCR	RIPTION			ST DE	S¢ NL	Pe SF	z	R %	žΰ	P≥g	Δŭ	LL	PL	PI
859.8_		Medium Sti (CL), Moist	ff, Brown SANDY LEAN ((FILL)	CLAY			_3.0	SS-1	3 3 3	8	56	18		4.0*			
	5	Stiff, Brown	SANDY LEAN CLAY (C	L) , Moist				SS-2	3 4 5	13	67	19		4.5*			
854.8_							_8.0	SS-3	4 4 4	11	72	23		4.0*			
852.8_	10_	Moist		J (CL),			_10.0	SS-4	4 5 6	15	100	20		2.0*			
050006CIN.GPJ CIL CORPORATE.GDT 5/16/18	- - 15_ - - 20_																
							AP					<u> </u>					
	2105 Schappelle Lane Cincinnati, Ohio 45240 Telephone: 513-722-8665 Fax: 513-834-6650 Email: ctlcin@ctleng.com				BORI HSA-Holl SFA-Soli RC -Roc MD -Muc MD -Was HA -Han	low S d Flig k Co d Dril sh Di nd Au	w⊨ I HC Stem A ght Au pring lling rilling uger	uger S ger S Cl B	SAMPLII S - Split S C - Shelb R - Rock S - Bag S	y Tube Core S ample	Samp Samp Sample	le * ple LL e PL PI SF Ng	Al - Har - Liqu - Plas - Plas - Plas - Stal 0 - Stal ormalized	DEREVIA ad Penetr uid Limit stic Limit sticity Ind ndard Pe ndard Pe I to 60%	omete ex netrati Drill Ro	on Tea	st

			TI	EST B	ORI	NG	REC	ORD)							
CLIENT	г	: Village W	est Alexandria						_		BO	RING NO	D.:	B-18	-18	
PROJE	СТ	: West Alex	andria WWTP						_		SHI	EET	1	0	=	1
LOCAT	ION	: 33 Desoto	Drive						_		DA	TE STAF	RTED	: 03-2	8-18	
PROJE	CT NO	. : 18050006	CIN								DA	TE COM	PLETED	: 03-2	8-18	
BORIN	G ELE	EVATION	: 866.0 Feet	RIG 1	YPE		: CME	45			DR	ILLER	:_[DS		
	NO	RTHING	: 641179.5180	CASI	NG DIA	۱.	: 3.25	"				MPERAT	URE : 4	0s		
	EAS	STING	: 1399275.6343		E SIZE		: N/A				WE	ATHER	:_0	Cloudy		
	DEF	PTH	: 10.0 Feet		MER		: Auto)			-					
	BO	RING METHO	D: HSA	ENEF	rgy Ra		: 84.1									
GROU	NDWAT	ER: En	countered at <u>None</u> At	completio	n <u>Dry</u>	1					1	1				
RATUM EVATION	MPLE EPTH					RATUM EPTH	MPLE	T "6"	0	ECOVERY	DISTURE	DTAL UNIT EIGHT f	JCONF. DMP., ksf	ATT L	ERBE	RG
ШST	SA		SOIL/MATERIAL DESCRIP	ΓΙΟΝ		ST	S N	, Ц a	z	8	Σŭ	P≥g	Ξŭ	LL	PL	ΡI
860.5_	-	Medium St CLAY (CL)	iff to Stiff, Brown SANDY LE , , Moist	AN		5.5	SS-1 SS-2	2 3 3 5 5	8	94	18		5.0* 5.0*	42	17	25
856.0_		Dense, Bro GRAVEL a BOTTOM (own WELL GRADED SAND v nd SILTY CLAY (SW-SC), M DF BORING	vith oist		10.0	SS-3 SS-4	8 10 12 10 15 14	31	56	7					
18050006CIN.GPJ CTL CORPORATE.GDT 5/16/18	- - - 15 - - - 20															
8 		0405.0	abannalla Lana	В	ORING	METH	OD	SAMPLI	NG ME	THOD		Α	I BBREVIA		6	
	TL ering ź	Cincinn Teleph Fax: 5 Email:	cnappelle Lane nati, Ohio 45240 one: 513-722-8665 13-834-6650 ctlcin@ctleng.com	HSA- SFA- RC - MD - WD - HA -	Hollow Solid F Rock C Mud Di Wash I Hand A	Stem A light Au Coring rilling Drilling Auger	Auger S ıger S C E	S - Split T - Shelt R - Rock S - Bag S	Spoon by Tub Core S Sample	Samp e Sam Sample e	le * ple LL e PL PI SF Ng	- Har - Liqı - Pla - Pla - Pla - Sta - Sta - Sta - Sta	nd Penetr uid Limit stic Limit sticity Ind ndard Pe ndard Pe d to 60%	omete lex netrati netrati Drill R	r on Te on od ER	st

APPENDIX B

RESULTS OF SOIL LABORATORY TESTS





























0.0	2.0	4.0	6.0	8.0 Strain (%)	10.0	12.0	14.0	16.0
				ENGINEERING Z				

APPENDIX C

BORING LOCATION PLAN & SOIL PROFILES







